

VACUUM DEPOSITED OPTICAL PHASE FILTERS

by

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ABSTRACT

The advantages of an optical spatial phase filter constructed by thickness variations are put forward and a method of fabricating such a device using vacuum deposition techniques is detailed.

The design and construction of a vacuum system to produce such a device is outlined. The system comprises a vacuum chamber with a source holder for zinc sulfide, an electronically controlled shutter, an aperture, and a substrate and holder mounted on an x-y motion table driven by stepper motors. The system is controlled by a mini-computer and measurements of thickness are made by an ellipsometer controlled by the minicomputer.

Experiments conducted with the system determine the spatial resolution and closed loop control capabilities to be adequate. An analysis of the results of the tests concludes that with further refinements it seems feasible to fabricate spatial phase filters by using vacuum deposition techniques.

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INTRODUCTION

This thesis is an investigation of the practicality of producing optical phase filters using vacuum deposition techniques.

Consider an optical system consisting of two parallel planes separated by some distance. The electromagnetic field intensity in one plane is a function of the intensity in the other plane. To produce specific intensity functions in one plane from a particular intensity function in the other requires, in general, a complex valued filter to be placed between the two. An example of such a filter is a lens.

An ideal lens can be represented mathematically as a multiplicative factor of the form,¹

$$\exp -jc(x^2+y^2) \quad (1)$$

where c is a constant and x, y are perpendicular reference axes. It is desirable to be able to produce more complicated phase functions than that of the lens. In fact, the corrections that must be made to a real lens so that it approximates the ideal more closely require a much more complex phase function.²

A simple form of phase filter was used by Tsujiuchi to correct lens aberrations and to produce optical systems with two focii.³ The filters used were very simple in that they consisted only of a pattern of half wavelength retardations. Approximations were made in the calculations of the filter pattern in order to easily fabricate the devices.

Recently holographic techniques have been used to produce phase filters.⁴ In the referenced work the authors used an amplitude hologram. Less than ten per cent of the signal power was deflected into the beam that has the desired altered phase.⁵

The most straightforward method of producing a pattern of phase variation would seem to be the use of a transparent material with a pattern of thickness variation. The material must have an index of refraction different from the transmission medium so that the speed of light is different in the filter. Thus the thickness variations convert to phase variations. With the aid of an index matching layer a phase filter of this type passes all of the available input signal power and is thus a significant improvement over the holographic type of filter. The thickness variation type of phase filter could conceivably be used in many applications in the field of optical information processing and spatial filtering where conventional photographic holograms are now used.

Researchers at I.B.M. have produced thickness variation phase filters which they call Kinoforms.⁶ The devices are constructed by bleaching computer generated photonegatives. Bleaching removes the dark material in the negative, leaving a transparent pattern of thickness. It is pointed out that the ideal way of fabricating such devices would be to produce the thickness directly and not rely on a transformation from

intensity to phase.

In this thesis an investigation is made of a method of fabricating a two dimensional device with thickness variations suitable for use as a phase filter in an optical system.

Starting with a parallel faced slab or substrate of transparent material, additional material must be added or removed to produce a thickness variation over the surface. Removal of material was not further explored, although developments in laser etching techniques make it look feasible. There are a number of methods of adding material to a substrate such as vacuum deposition, sputtering and screening. Of these, vacuum deposition seemed to be the most promising technique and was singled out for investigation.

Vacuum deposition was chosen for further study for a number of reasons. The technique has been used widely in the field of optics for various purposes such as anti-reflection films and multi-layer frequency selective filters. The materials used in vacuum deposition have been studied and are well documented.^{7,8,9,10}

The following chapters describe the work performed to investigate the feasibility of fabricating phase filters by vacuum deposition techniques. Chapter I is a description of the proposed filter and the method of production. Chapter II describes the hardware designed and constructed, and the software written. Chapter III is a summary of the results and conclusions of the investigation.

CHAPTER I - BACKGROUND

A dielectric material will cause a phase change of the light transmitted through it in the following way. Consider Figure 1(a). The optical system between the two fixed reference planes z_0 and z_1 can be considered as a system with a transmission coefficient T .

$$T = \frac{(1+r_{01}r_{12}+r_{01}+r_{12})}{1+r_{01}r_{12}} e^{-j(\theta_1+\theta_2+\theta_3)} \quad (2)$$

r_{ij} is the Fresnel reflection coefficient from medium i to medium j. The reflection coefficient for perpendicularly polarized light is

$$r_{ij} = \frac{n_i \cos \phi_i - n_j \cos \phi_j}{n_i \cos \phi_i + n_j \cos \phi_j} \quad (3)$$

and for parallel polarization

$$r_{ij} = \frac{n_i \cos \phi_j - n_j \cos \phi_i}{n_i \cos \phi_j + n_j \cos \phi_i} \quad (4)$$

ϕ_i and ϕ_j are defined in Figure 2. The optical path lengths θ_i 's are given by

$$\theta_i = \frac{2\pi}{\lambda} n_i d_i \cos \phi_i \quad (5)$$

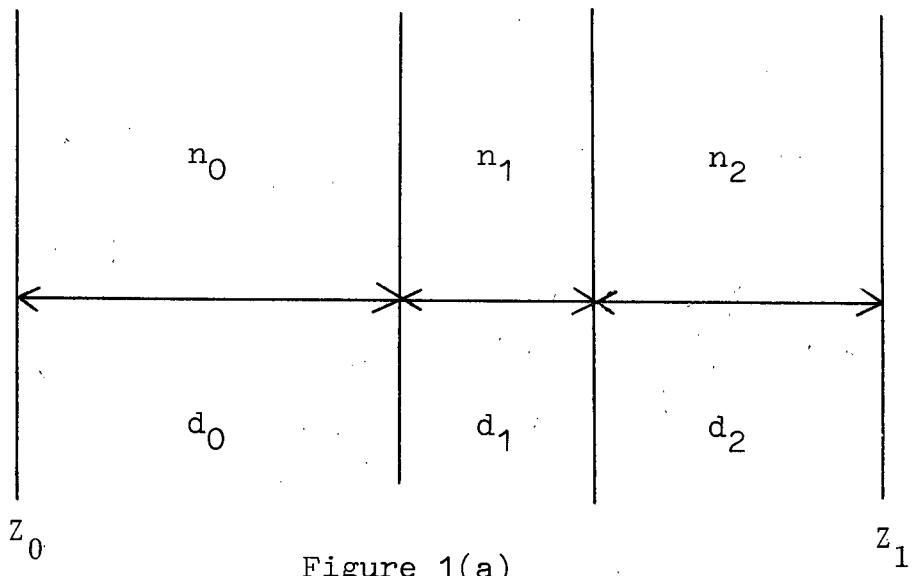


Figure 1(a)

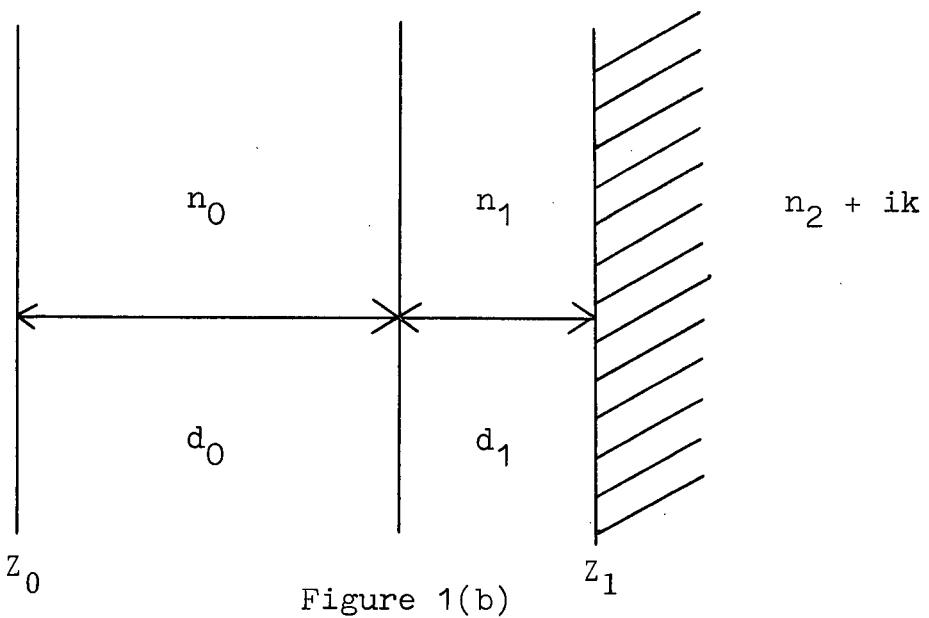


Figure 1(b)

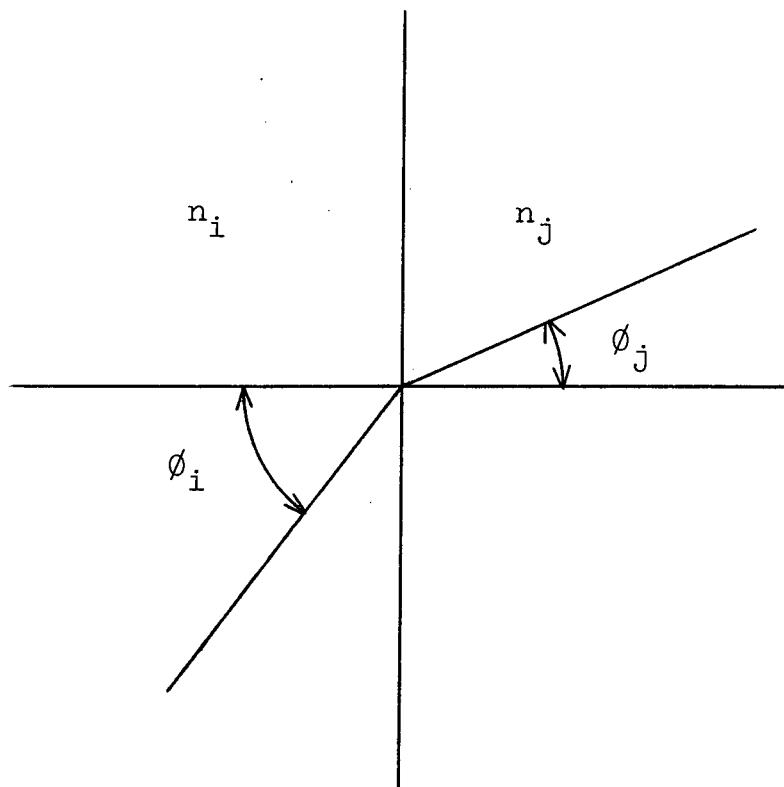


Figure 2. Angle of Incidence

where λ is the wavelength of the light, n_i is the refractive index of the i^{th} medium, and d_i is the thickness of the i^{th} medium. By varying the thickness d_1 , the phase change introduced by the optical system is altered.

A similar result can be achieved by using the reflection geometry of Figure 1(b). The optical system between the two planes z_0 and z_1 can be characterized by a reflection coefficient

$$R = \frac{(1+r_{01}+r_{12}+r_{01}r_{12})(r_{01}+r_{12}e^{-j2\theta_1})}{1+r_{01}r_{12}e^{-j2\theta_1}} e^{-2j\theta_0} \quad (6)$$

The computer program in Appendix I was used to calculate the phase changes produced by varying the thickness of the dielectric layer. The arbitrary zero of phase change was chosen to occur when the dielectric layer has zero thickness. Appendix I lists the computed change of phase due to dielectric thickness.

For the transmission geometry, the optical constants used in the equations were chosen for a film of magnesium fluoride on glass in air. For the reflection geometry, the constants used correspond to a film of zinc sulfide on an aluminum backing in air. These constants were chosen because they represent materials that have been frequently used in the field of optics.

A phase filter, being a device which alters the phase of a plane wave as a function of two dimensions, could be

used in much the same manner as an interference hologram to store information and create images. This property can be demonstrated by utilizing the Fourier transformation property of a lens. A lens displays the two dimensional spatial Fourier transform of the intensity of one of its focal planes in the other focal plane. Thus, if an image is placed in the focal plane of a lens, its Fourier transform would appear in the other focal plane. The Fourier transform of a real image is in general a complex valued function.

The amplitude part of such a function can be easily constructed with a photographic transparency. If a phase filter could be constructed with the appropriate pattern of phase, one should be able to produce an image from the complex valued Fourier transform. Even without the amplitude part of the filter, it should be able to produce a reasonable image. This experiment was simulated numerically by using the Fast Fourier Transform program available on the University of British Columbia I.B.M. 360 computer system.

A two dimensional black-white image was digitized and then transformed into the spatial frequency plane. There the individual spatial frequencies were altered by normalizing each amplitude to unity while leaving the phases intact. This simulates the effect of illuminating the phase filter without amplitude compensation with a unit amplitude plane wave. The Fourier transform of the altered transform was then taken. This corresponds to the reconstruction process with a lens. Taking the Fourier transform twice,

instead of taking the transform and its inverse, results in the axes being inverted.

The program written to demonstrate this effect is listed in Appendix II. The input to the program is the digitized pattern of Figure 3(a). The intensity function is spread by the amplitude normalizing. However, the bright areas, as indicated by the pattern of Figure 3(b), still show a reproduction of the original. The results of the computer experiment demonstrate the capabilities of a phase filter.

Vacuum deposition requires that the material to be deposited be heated to the vapour state and then condensed on the substrate. To produce a phase filter with vacuum techniques, involves the deposition of a varying thickness dielectric on the surface of a substrate such that the thickness is a function of the position on the surface. This involves controlling the position of deposition and also controlling the thickness of deposition.

Position of deposition can be controlled by collimating the vapour from the deposition source into a narrow beam and exposing the substrate only to that beam. The substrate must then be moved about so that the beam covers the entire surface. Use of this method restricts the spatial resolution to the fineness of the beam. An ellipsometer was available to measure the thickness of the deposited layer. The measurements from the ellipsometer could be used to determine the thickness of the layer that was currently being deposited

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Original Image

Figure 3(a)

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Second Transform

Figure 3(b)

and thus indicate when the layer was thick enough before proceeding to the next area.

The ellipsometer had been previously automated by connecting it to a Digital Equipment Corporation PDP 8-e minicomputer. This computer was ideally suited to control the positioning of the substrate and to control the thickness of the deposition at any one point. It would also be simple to communicate the pattern of phase required to a minicomputer since the pattern would, in all probability, be generated by a large computer.

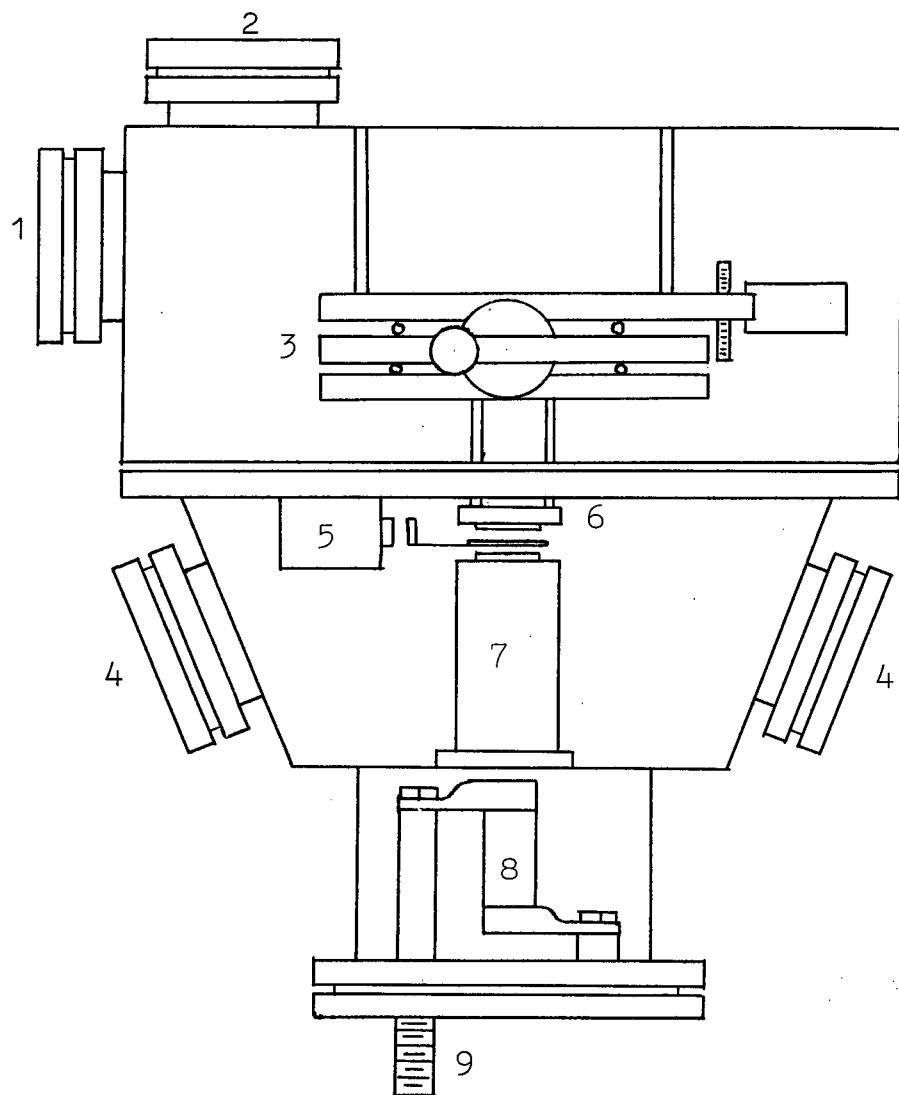
To further investigate the feasibility of producing phase filters by vacuum techniques, additional apparatus had to be designed, constructed and tested. The control strategy had also to be designed and implemented.

CHAPTER II - HARDWARE AND SOFTWARE

The technique of vacuum deposition requires a chamber equipped with a pumping system that can maintain pressures lower than 1×10^{-5} Torr. In this chamber, the source material to be deposited must be heated to a high temperature so that it vaporizes. The substrate must be held in proximity to the source so that the vapour condenses on its surface. Figure 4 is a sketch of the vacuum system designed and built to test the feasibility of producing a pattern of varying thickness deposit.

The main section of the chamber houses an x-y movement upon which the substrate is mounted. The x-y movement is driven by two stepper motors mounted within the chamber and powered from an electrical feedthrough on the side of the chamber. The rear of the chamber has a connection to the pumping system.

The front section of the chamber has angled sides and a barrel shaped nosepiece. The sides, which form a "V" with an interior angle of 140 degrees, are fitted with windows such that a light beam entering the center of one window at right angles would strike the substrate at an angle of incidence of 70 degrees and reflect out the other window. An electromagnetically operated shutter is fitted along the center line of the chamber as close to the point of intersection with the right angles to the windows as possible without interfering with the passage of light from



- 1 - electrical feedthrough
- 2 - vacuum pump connection
- 3 - x-y motion table and drive motors
- 4 - optical windows
- 5 - shutter
- 6 - substrate holder
- 7 - collimator
- 8 - source
- 9 - high current feedthrough

Figure 4. Vacuum Chamber Details

window to substrate to window. Between the shutter and substrate is a mask with a square aperture. The barrel of the chamber contains the source. The source is a round tantalum tube that is connected to high current electrical feedthroughs at the end of the barrel. The endpiece also contains an electrical feedthrough for the operation of the shutter. The source shutter and mask all lie along the center line of the chamber. Thus, the source is only able to deposit material on that section of the substrate visible to the source through the mask and then, only when the shutter is open. The motion of the x-y movement presents different areas of the substrate to the source.

The windows are fitted in such a way that the entire chamber can be placed between the two arms of an ellipsometer. Thus, the thickness of the area being deposited can be monitored in situ.

The chamber is constructed of helium-arc welded type 316 stainless steel. The front section separates from the main chamber to allow servicing of the substrate. The two sections are bolted together and sealed with a large "O" ring. The source and feedthroughs are mounted on a flange that is bolted to the front end of the barrel section. The entire chamber is mounted on a large aluminum plate that facilitates locating the unit on the ellipsometer.

The pumping system connected to the rear of the main chamber consists of a mechanical rotary pump for roughing from atmospheric pressures and an oil diffusion pump for

higher vacuums. This arrangement of pumps is able to adequately maintain a pressure of less than 1×10^{-5} Torr.

The chamber and x-y movement were designed for this experiment. The construction was carried out by Mr. J. Stuber.

The ellipsometer used to monitor film thickness had been previously equipped to make measurements under control of a minicomputer. An ellipsometer is a device which measures two optical quantities called Δ and Ψ which are related to the reflection coefficients of an optical system by

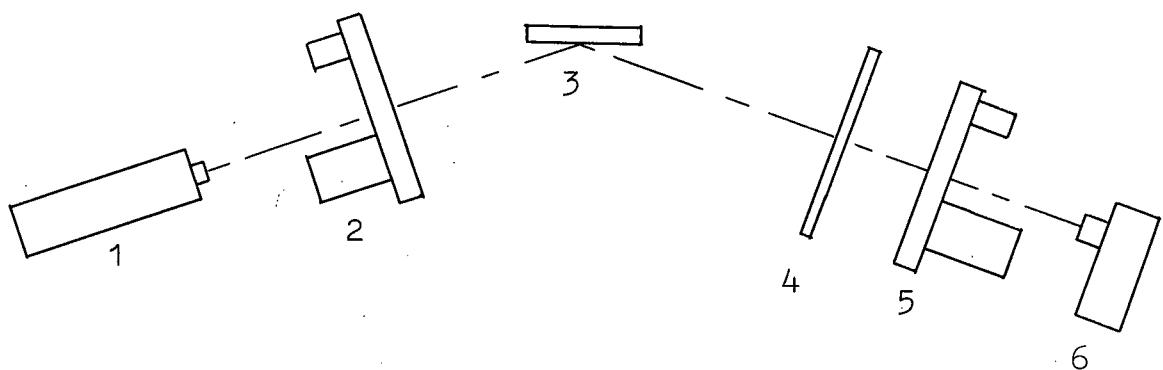
$$\tan \Psi e^{j\Delta} = \frac{R_p}{R_s} \quad (7)$$

where R_p is the reflection coefficient for parallel polarized light and R_s is the reflection coefficient for perpendicular polarized light.

A schematic diagram of the ellipsometer is given in Figure 5. The polarizer and analyzer are polaroids and the quarter wave plate is a Soleil Babinet compensator that introduces a phase change of 90 degrees between the perpendicular and parallel polarizations of the light beam. The intensity of the light emerging from the analyzer is given by

$$I = I_0 \sin^2(\Psi + A) - \sin 2\Psi \sin^2 \frac{1}{2}(\Delta - \Delta') \quad (8)$$

Δ' is defined by



- 1 - laser light source
- 2 - polarizer with shaft encoder and drive motor
- 3 - sample
- 4 - quarter wave plate
- 5 - analyzer with shaft encoder and drive motor
- 6 - photomultiplier tube light detector

Figure 5. Ellipsometer Schematic

$$\tan \Delta' = \sin \delta \tan(2P - \frac{\pi}{2}) \quad (9)$$

where δ is the retardation of the quarter wave plate, and A is the analyzer setting and P is the polarizer setting.

Making a measurement with the ellipsometer, or balancing the ellipsometer, involves determining a combination of polarizer and analyzer settings that produces a null in the light intensity emerging from the analyzer.

With the quarter wave plate set at -45° to the plane of incidence, at extinction the relations between Δ and P, and Ψ and A are:

$$\begin{aligned} \Delta &= 90^\circ - 2P & 135^\circ > P > -45^\circ \\ \Psi &= A & 90^\circ > A > 0 \end{aligned} \quad (10)$$

and

$$\begin{aligned} \Delta &= 2P - 90^\circ & 225^\circ > P > 45^\circ \\ \Psi &= 180^\circ - A & 180^\circ > A > 90^\circ \end{aligned} \quad (11)$$

A detailed list of all combinations of analyser and polarizer settings that produce a null is given by F.L. McCrackin et al.¹²

Because the signal from the photomultiplier falls to insignificant levels near a null, it was not possible to determine the position of the null directly. Fortunately, both I versus A and I versus P characteristics are symmetrical about the null point. I versus P is symmetrical provided δ is close to 90 degrees. Thus, by determining equal intensities on either side of the minimum, the position of the null can be determined as the midpoint.

Both the polarizer and analyzer are driven by stepping

motors geared so that one step rotates the polaroid by 0.01 degrees. The positions of the polarizer and analyzer are measured by a shaft encoder connected to the drive gearing in each unit. The two encoders are read by a multiplexed decoder to provide a five digit BCD output which ranges from 000.00 degrees to 359.99 degrees. The analyzer shaft encoder was mounted in opposition to the scale engraved in the analyzer so that the reading from the encoder must be complimented by 360 degrees to make it compatible. The light intensity monitored by the photomultiplier is read through a multiplexed ten bit analog to digital converter.

The ellipsometer had previously been interfaced to a PDP-8e minicomputer. The shaft encoder and photomultiplier were input to the computer and the computer was able to turn the stepper motors on the analyzer and polarizer. The interface was expanded so that the computer was able to rotate the stepper motors connected to the x-y drive in the vacuum chamber. The shutter was also operated through the computer interface.

Operator communication to the system was made via an ASR-33 teletype. The teletype handler program operates the teletype under interrupt control. All input from the keyboard is put into a buffer until it is used and removed by a program requiring input. All print output is put into another buffer which the teletype handler tries to keep empty by outputting the contents on the printer. Since teletype input and output are performed on an interrupt basis, the

computer is able to carry out control tasks in the background while serving the teletype.

A simple operating system was written to allow an operator to initiate control actions from the keyboard. When first started, the operating system initializes flags and counters used throughout the programs in the system. The only other function of the operating system is to check the keyboard buffer for inputs and translate these inputs into control programs to execute. Commands take the form of two truncated ASCII characters. The operating system compares inputs with a table of names it recognizes. If a match is made, the control program in the address table corresponding to the name table is executed. The control programs are all subroutines that return to the operating system when they have completed their task.

For this thesis, it was required to operate the ellipsometer and the shutter and x-y drive in the chamber. Also a higher level program was required to coordinate these controls in such a way as to produce a deposit of a required thickness. Two commands that were implemented were "set the polarizer" (SP), and "set the analyzer" (SA). Either command expected a five digit input from the keyboard that represented the position required of the analyzer or polarizer. These two programs first read the shaft encoder to determine the present position of the unit and then output the appropriate number of steps to turn the unit to the required position in the direction that required the

least motion.

The two commands to move the x-direction and y-direction stepper motors on the x-y drive in the chamber were given the names MX and MY respectively. The programs associated with these commands expected inputs from keyboard to indicate direction of movement in the plane and the distance of travel. Direction was indicated by "F" and "R". An "F" meant to the right in the x-direction and up in the y-direction when looking at the chamber from the source end. "R" is the opposite of "F".

All four stepper motors, the shaft encoder multiplexer and the shutter switch were connected to device 33 in the computer interface. This device was a set of twelve flip flops, one per bit of the computer word as defined in Table 1. The IOP2 pulse from the computer output the accumulator to set the flip flops. The IOP4 pulse was used to send a pulse to the stepper motors that had their enable bit set. The pulse was steered to the clockwise or counter-clockwise input on the stepper motor controllers by the direction bit. Thus, any of the four stepper motors could be moved by first setting its enable and direction bits with an IOP2 pulse and then sending an IOP4 pulse for each step.

Once the gating for a motor had been set, a routine labelled STEP was used to output one step pulse to the motor. The motors used had a resonance at approximately 200 steps per second. To run the motors at a speed above the resonance required that they be accelerated from a stopped position.

Device 33 of Computer Interface

<u>Bit Position</u>	<u>Function</u>
0	Polarizer motor direction
1	Polarizer motor enable
2	Analyzer motor direction
3	Analyzer motor enable
4	Y-axis motor direction
5	Y-axis motor enable
6	X-axis motor direction
7	X-axis motor enable
8	Unused
9	Unused
10	Shutter control
11	Shaft encoder gate

Table 1

Since timing was generated by software, it was not convenient to run more than one motor at a time. The hardware status of device 33 was stored in a location labelled DIR. Bit 9 of DIR was used for a flag to indicate that acceleration was required. The routine STEP accelerated the motors by shortening the time between pulses from a maximum when the flag was first set to a minimum after a certain number of pulses had been sent. At this time the flag was cleared.

The output of the multiplexed shaft encoder was connected to device 30 in the interface. The shaft encoder was always set to read the analyzer when the analyzer motor was selected, and the polarizer, when the polarizer motor was selected. The IOP2 pulse was used to strobe the high order two BCD digits into the accumulator and the IOP4 pulse was used to strobe the three low order BCD digits. These numbers were read by a program named RDSFT and were stored in locations SHFTH and SHFTL respectively.

The output from the photomultiplier on the ellipsometer was measured by the computer with an analog to digital converter, device 32 in the interface. The program, ANALG, was responsible for reading the analog to digital converter and converting the reading into volts.

To take a reading from the ellipsometer requires that the polarizer and analyzer be positioned so that the output from the photomultiplier is a minimum. The suggested procedure is to first balance, that is, find a minimum of, the polarizer.¹¹ Then the analyzer is balanced. The

polarizer is again balanced and finally the analyzer is balanced again. This procedure can be commanded from the keyboard with a BE input. The procedure is really a combination of the two commands BA and BP which balance the analyzer and polarizer respectively. These two routines set the gating for the appropriate stepper motors and then call upon a common routine called BALU.

The routine BAL (see Figure 6) determines the position of a minimum photomultiplier reading by finding equal intensities around a minimum. To avoid noise problems due to low signal levels, the sum of many readings is taken. First a running sum of readings is taken by moving the motor one step, reading the photomultiplier and adding the reading to the sum. The sum is taken over sixty-four steps. A second running sum is taken and compared with the first. If the second sum is larger, the motor is reversed and the routine restarted. Otherwise, the first sum is replaced by the second and the second sum is taken again and again compared with the first. A flag is set to indicate the minimum has not yet been passed. At some point the second sum will be larger than the first indicating that the minimum has been passed. Another set of readings is taken and this sum is saved as the comparison on one side of the minimum. The motor is reversed and run back two sets of readings. The next set of readings is saved, reading by reading, along with the running sum. From here on, every time the motor is stepped, the newest reading is put at the beginning of the

FLOWCHART OF SUBROUTINE BAL

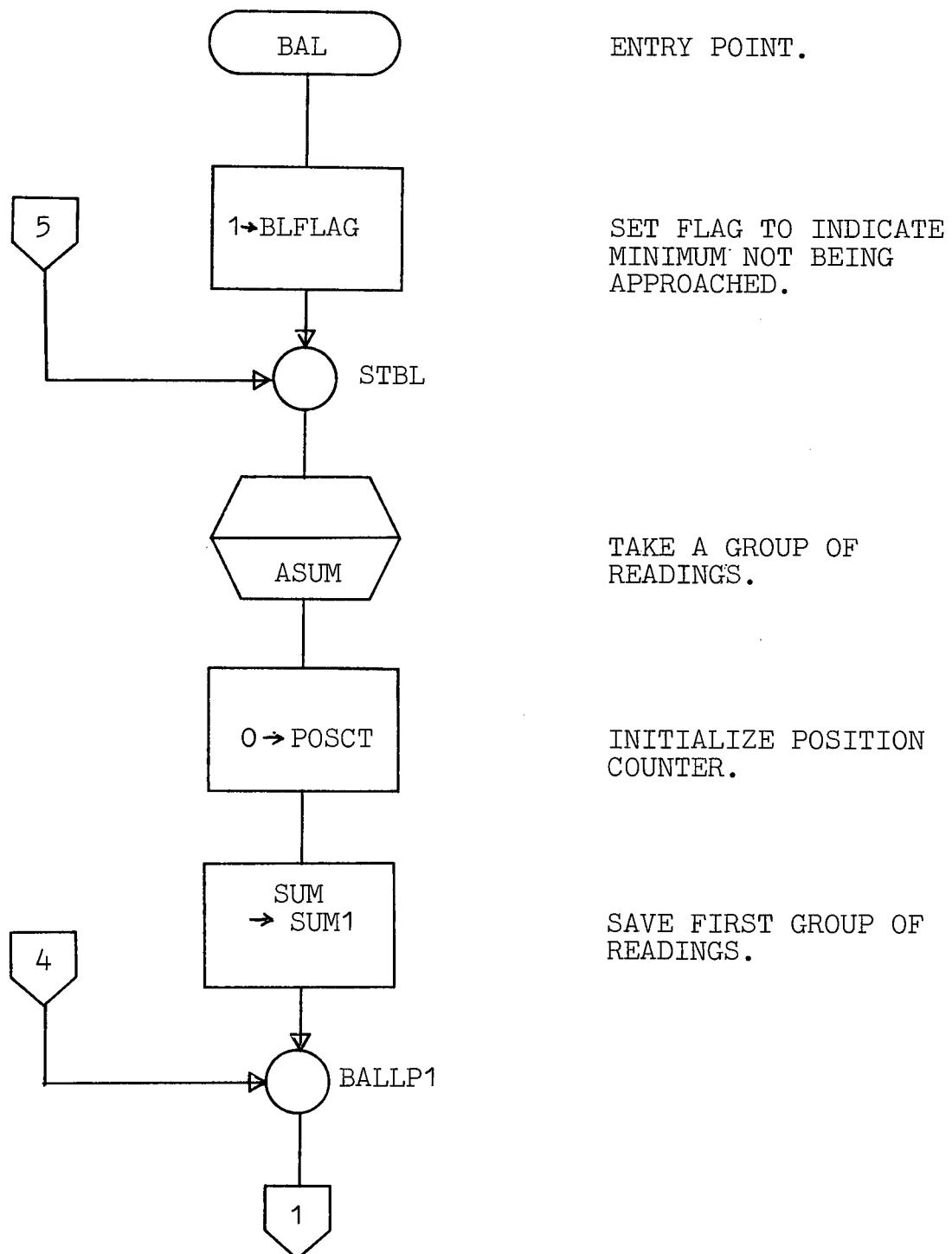
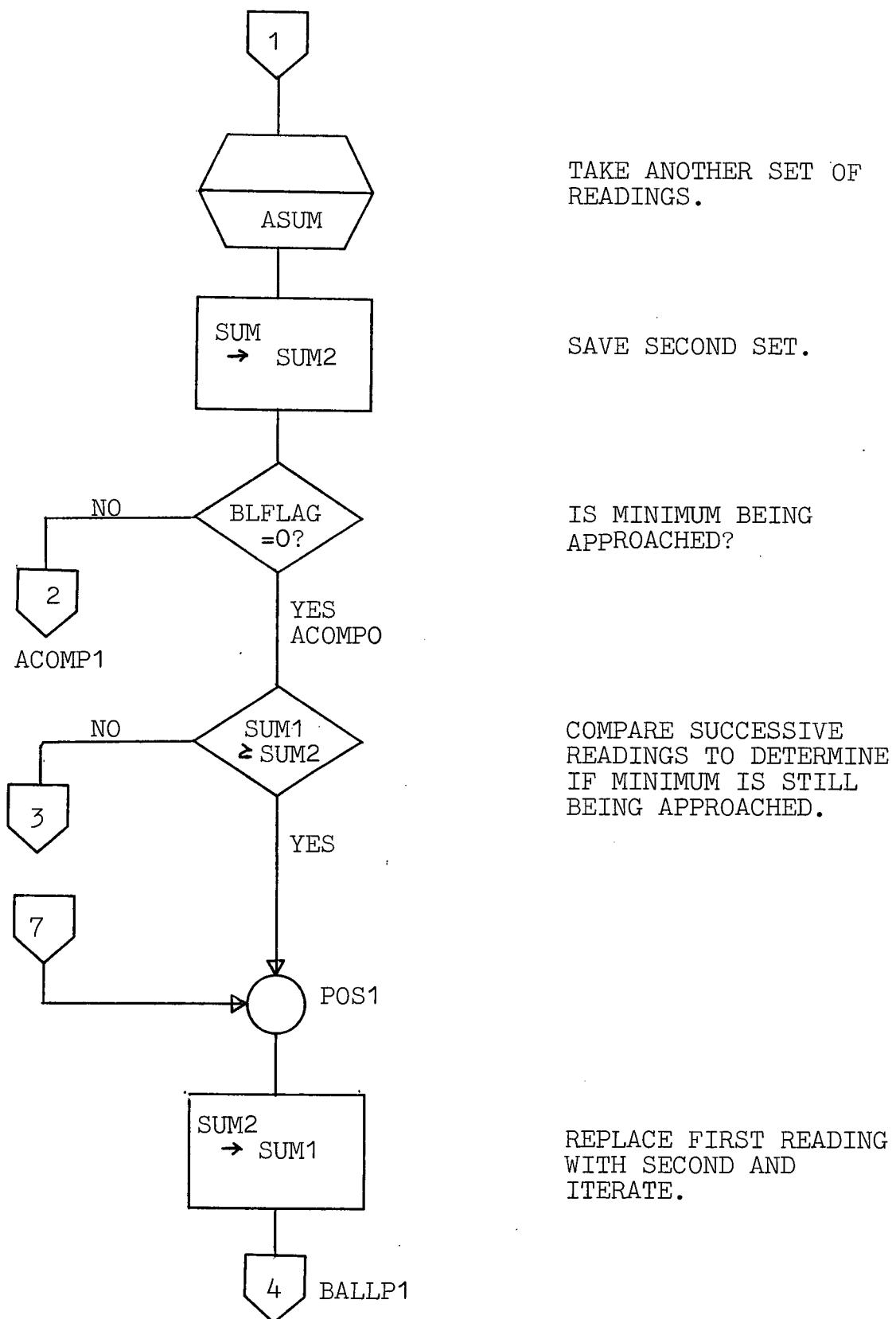
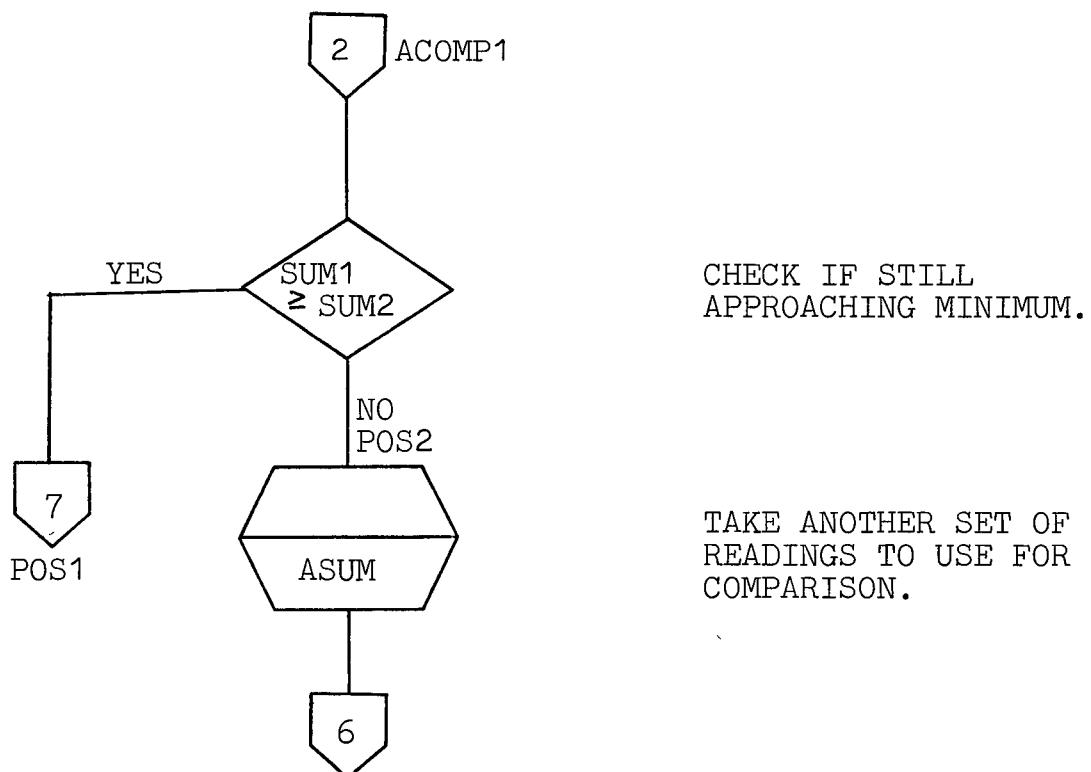
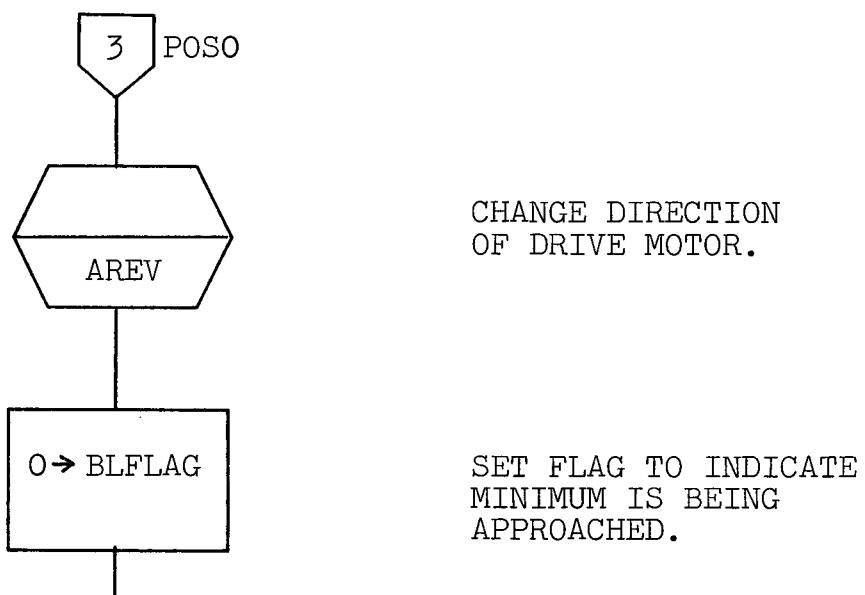
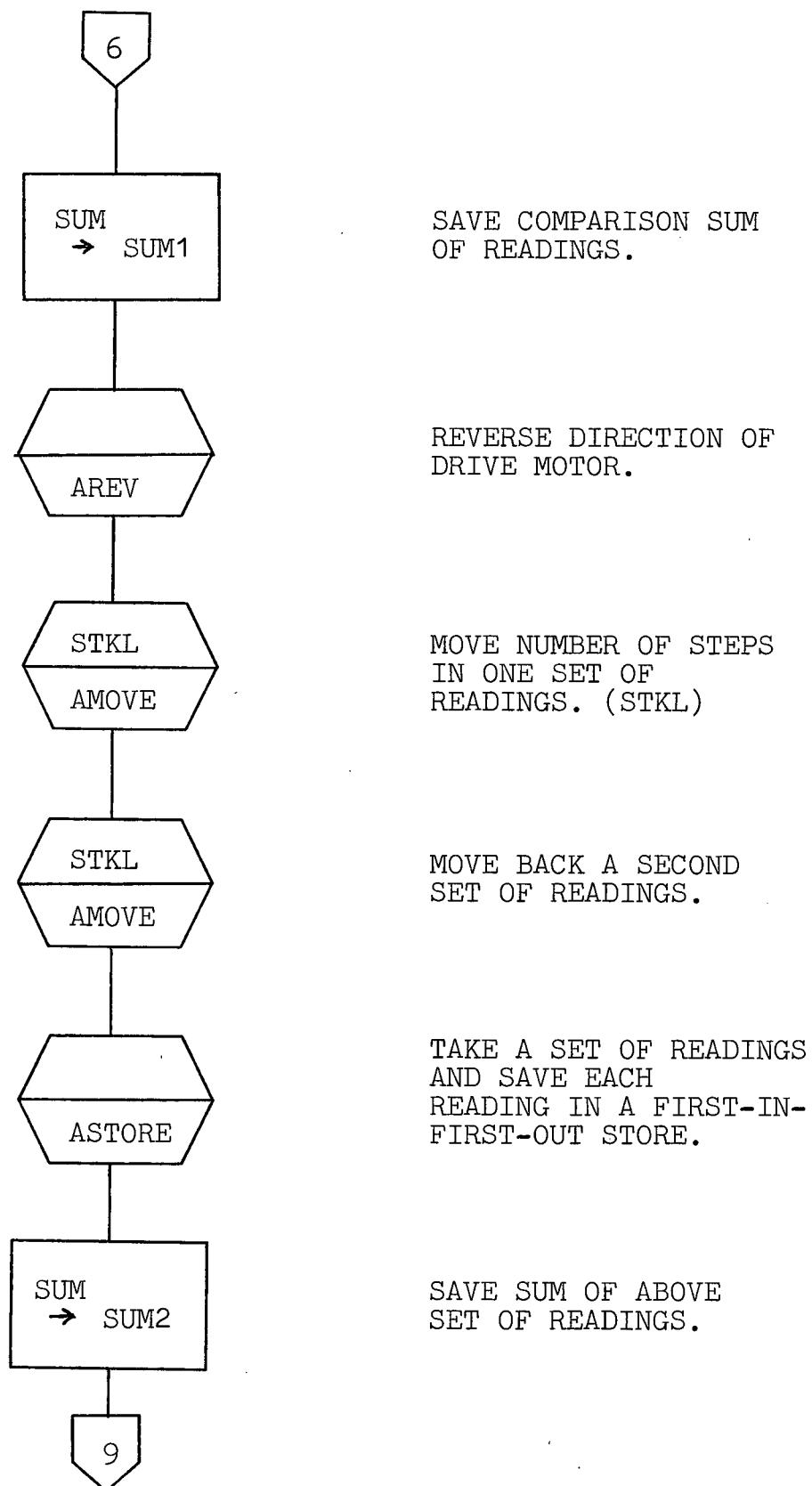
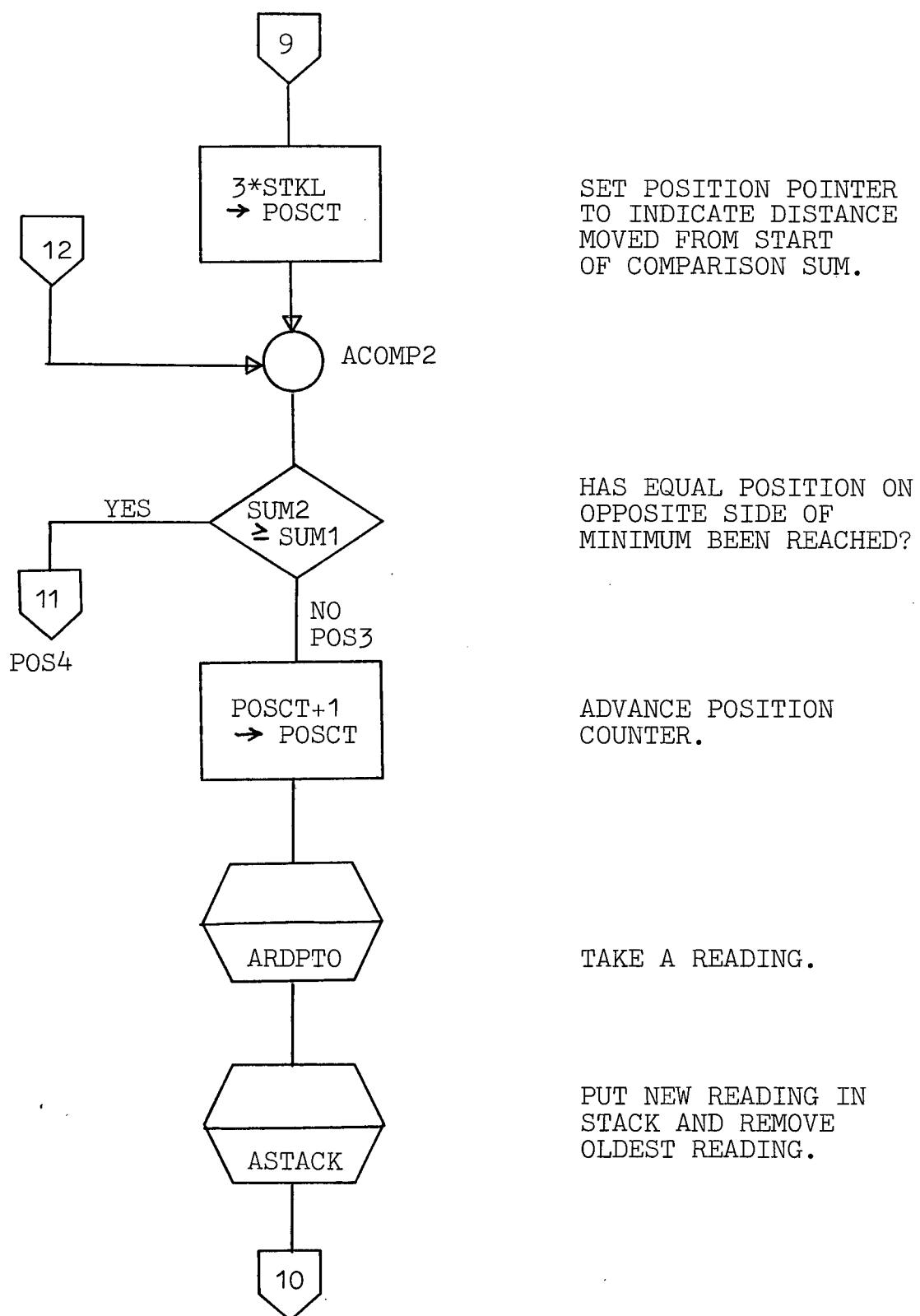


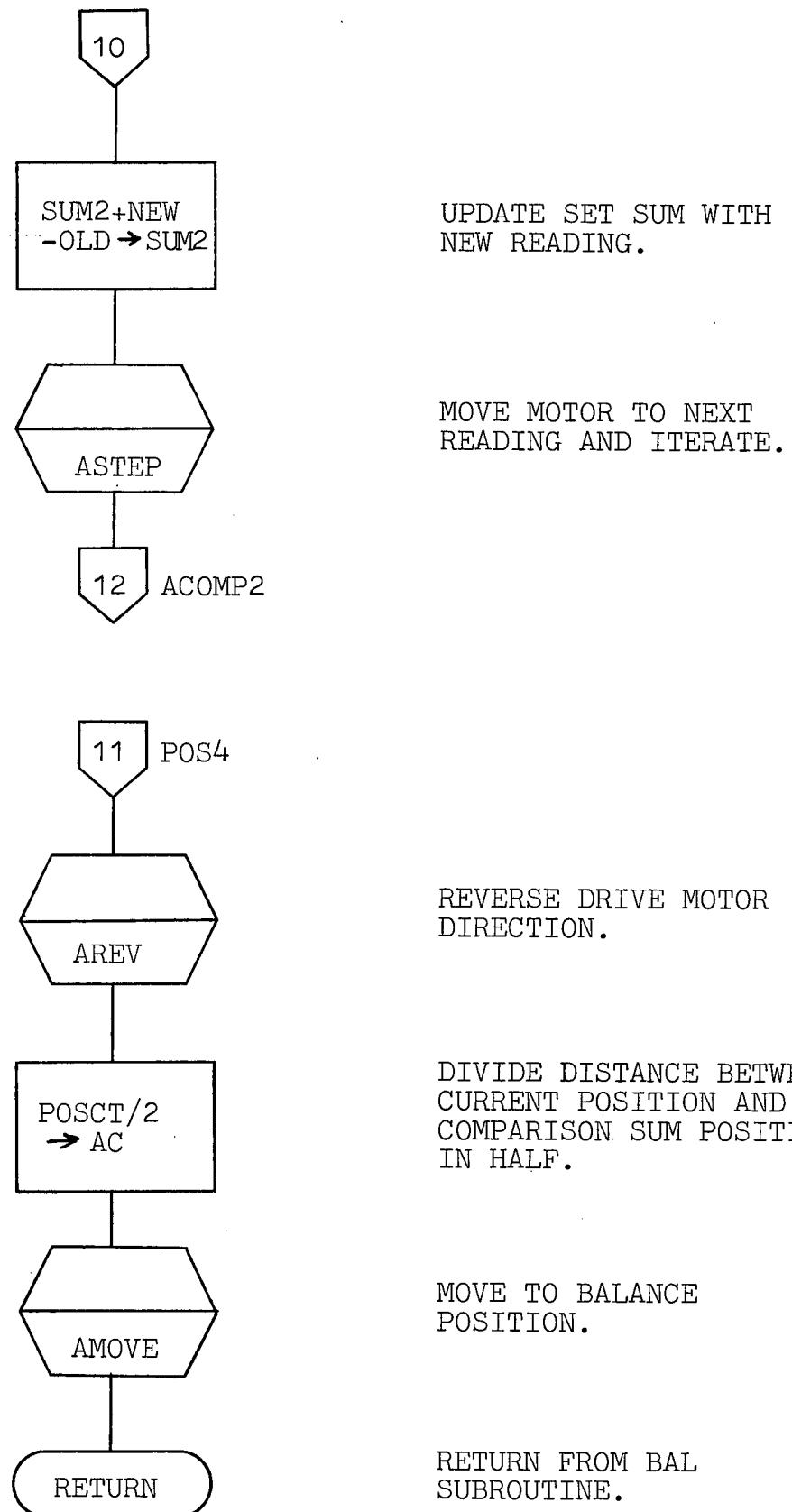
FIGURE 6











buffer and the oldest one is removed. The running sum is also adjusted by adding on the newest reading and subtracting the oldest. This running sum is compared with the comparison sum and as soon as it is equal to or larger than the comparison sum, the position of the minimum can be determined as the midpoint of the two sums. The motor is reversed and driven to the midpoint. The analyzer and polarizer positions and photomultiplier reading at the balance point are printed on the teletype.

The shutter in the chamber could be operated from the keyboard with the two commands "open shutter" (OS), and "close shutter" (CS). These commands changed the state of a flip flop on device 33 in the interface. The shutter solenoid was energized by a power transistor driven by the flip flop.

Closed loop control of film thickness was accomplished by setting the analyzer and polarizer to the positions at which a balance would occur if the film were the correct thickness. The shutter was then opened until the photomultiplier output dropped to a minimum. The shutter was closed to stop the deposition process. This procedure was commandable from the keyboard and given the name SB, "stop on balance". For noise immunity, the SB program uses sums of readings instead of a single reading of the photomultiplier.

A typical sequence of commands that produces a deposit of a specified thickness is the following:

MX F 001
MY F 001
SA 47.21
SP 325.54
SB

The MX and MY commands move the substrate to a desired position and the SA and SP commands move the analyzer and polarizer to the balance position. The SB command finally opens the shutter and closes it when a balance occurs. The distances for the MX and MY commands are in units of the mask aperture width so that adjoining areas can be reached by moving in increments of one.

The teletype input program was written so that the paper tape reader on the ASR 33 was enabled if there was room in the input buffer. Thus, the operation of the system could be controlled with commands stored on paper tape. In this way the thickness pattern of the substrate could be generated on a large computer system where it could be converted to analyzer and polarizer settings. The large computer system would then generate an ASCII paper control tape. The physical pattern could then be produced with the hardware described by reading this tape.

CHAPTER III - RESULTS AND CONCLUSIONS

To test the performance of the equipment, two experiments were conducted. The first experiment consisted of depositing material to study the deposition process and products. The second experiment was a check of the closed loop control of the system.

The substrate used was an optical glass flat, 25 x 25 millimeters. The substrate was coated with a layer of vacuum deposited aluminum to give it a reflecting surface. The substrate was transferred to the x-y movable holder in the vacuum chamber. The chamber was evacuated in preparation for deposition of zinc sulfide.

Before any depositions were made on the bare aluminum surface of the substrate, the surface was checked for uniformity. This was accomplished by moving the x-y holder so that the ellipsometer could take readings of different areas of the surface. A map of the surface uniformity is given in Table 2.

The x-y holder was then set to a corner of the substrate and the evaporation current turned on. The shutter was opened and zinc sulfide allowed to deposit through the aperture onto the substrate. The ellipsometer was used to observe the evaporation process. After a suitable thickness of zinc sulfide had been deposited, the evaporation was halted by closing the shutter. The x-y holder was then moved a distance equal to the width of the aperture,

56.85	56.69	56.50	55.76
46.18	46.18	46.16	46.21
57.03	56.82	56.59	55.85
46.19	46.19	46.15	46.24
57.41	57.30	57.00	56.57
46.17	46.18	46.21	46.20
57.76	57.56	57.42	56.85
46.11	46.17	46.10	46.27
58.88	58.64	58.01	57.17
46.03	46.03	46.05	46.08

Top - Polarizer

Bottom - Analyzer

Table 2. Scan of Aluminum Coated Substrate

1.59 millimeters. The shutter was then again opened to deposit onto an area adjacent to the first. A thickness of zinc sulfide different from the first area was then deposited on the second. The procedure was repeated for a third time to form three adjacent areas of different thicknesses.

After the third area, the shutter was closed and the x-y holder moved at right angles a distance twice the width of the aperture. At this position, a thickness of zinc sulfide was again deposited. The holder was then positioned a little beyond the edge of the last square deposited and an ellipsometer reading was taken. The holder was then moved a small distance, 47 micrometers, towards the square and another reading was taken. This process was repeated until the profile of the entire square was obtained. The holder was then positioned near the area of the three adjacent squares and a similar scan was made along the center line of the three squares. The readings are presented graphically in Figures 7, 8 and 9.

The second experiment was performed to determine the capabilities of the control system. For this experiment different areas of the same substrate were used. Suitable values of polarizer and analyzer readings were chosen from the first set of evaporations. These readings were used to produce a control tape for the second experiment. Four areas adjacent to one another were to be evaporated upon. The vacuum system was prepared and evacuated. After the

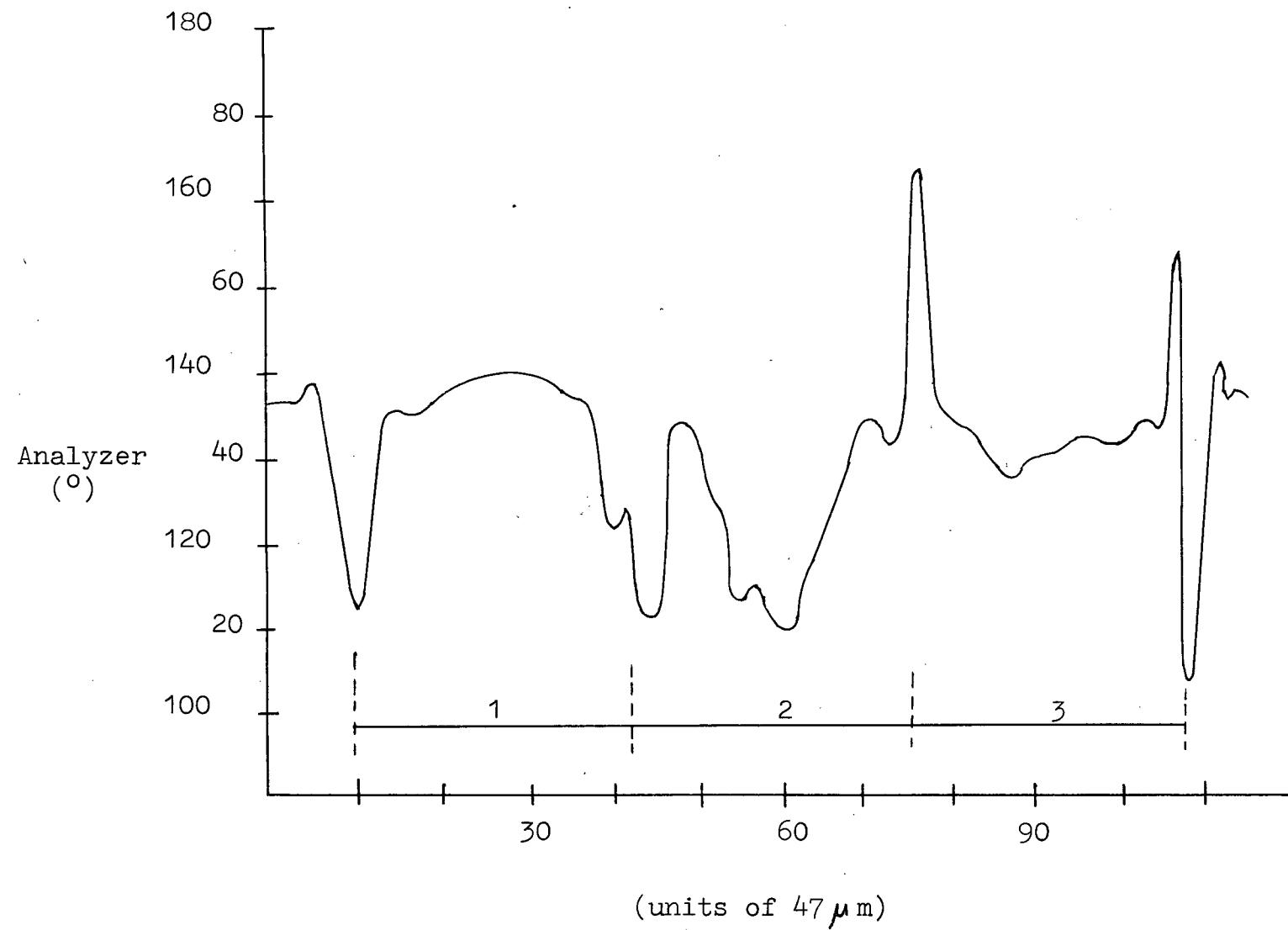
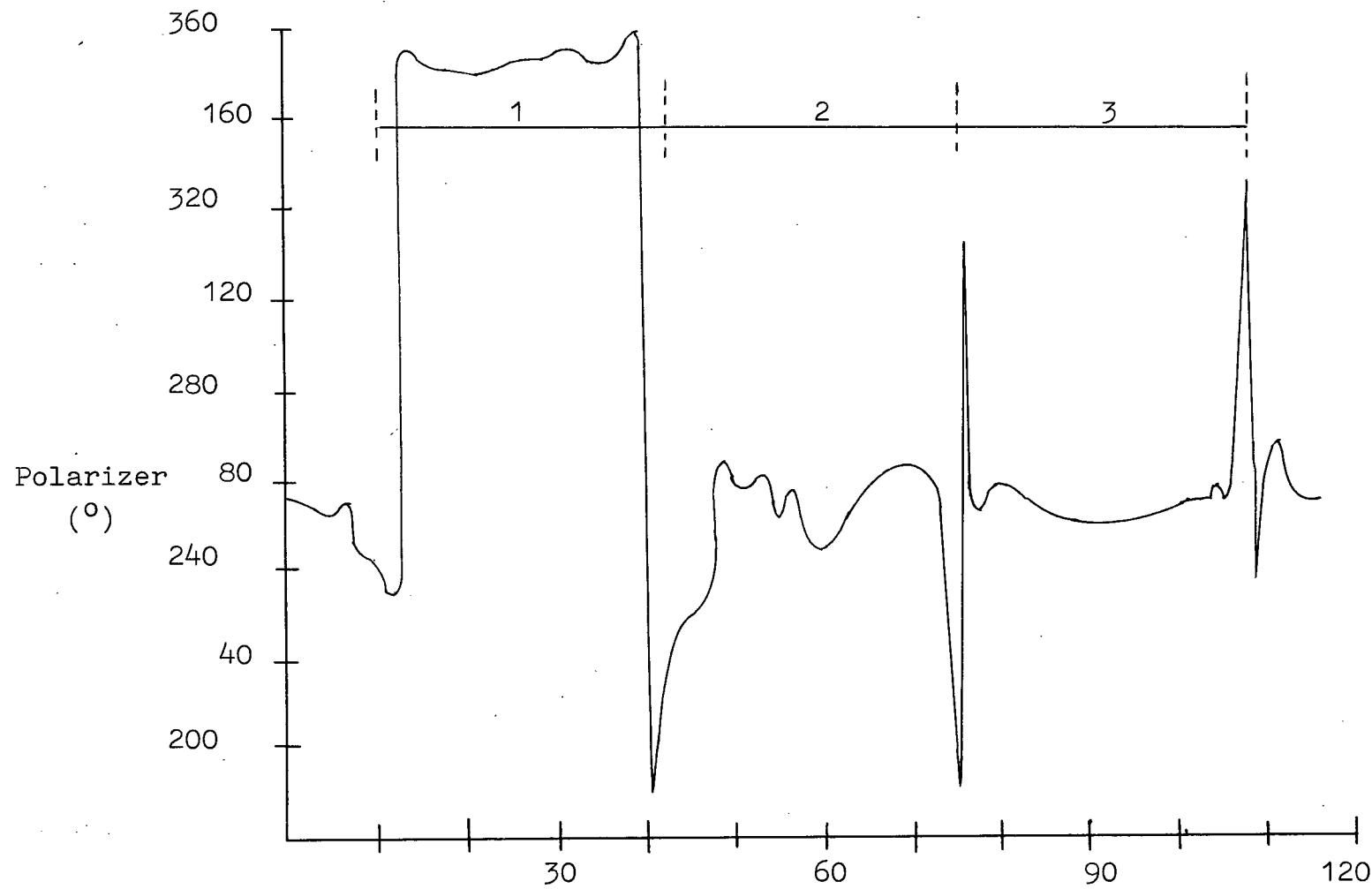


Figure 7. Analyzer Scan of Squares 1 - 3



(units of $47\mu m$)

Figure 8. Polarizer Scan of Squares 1 - 3

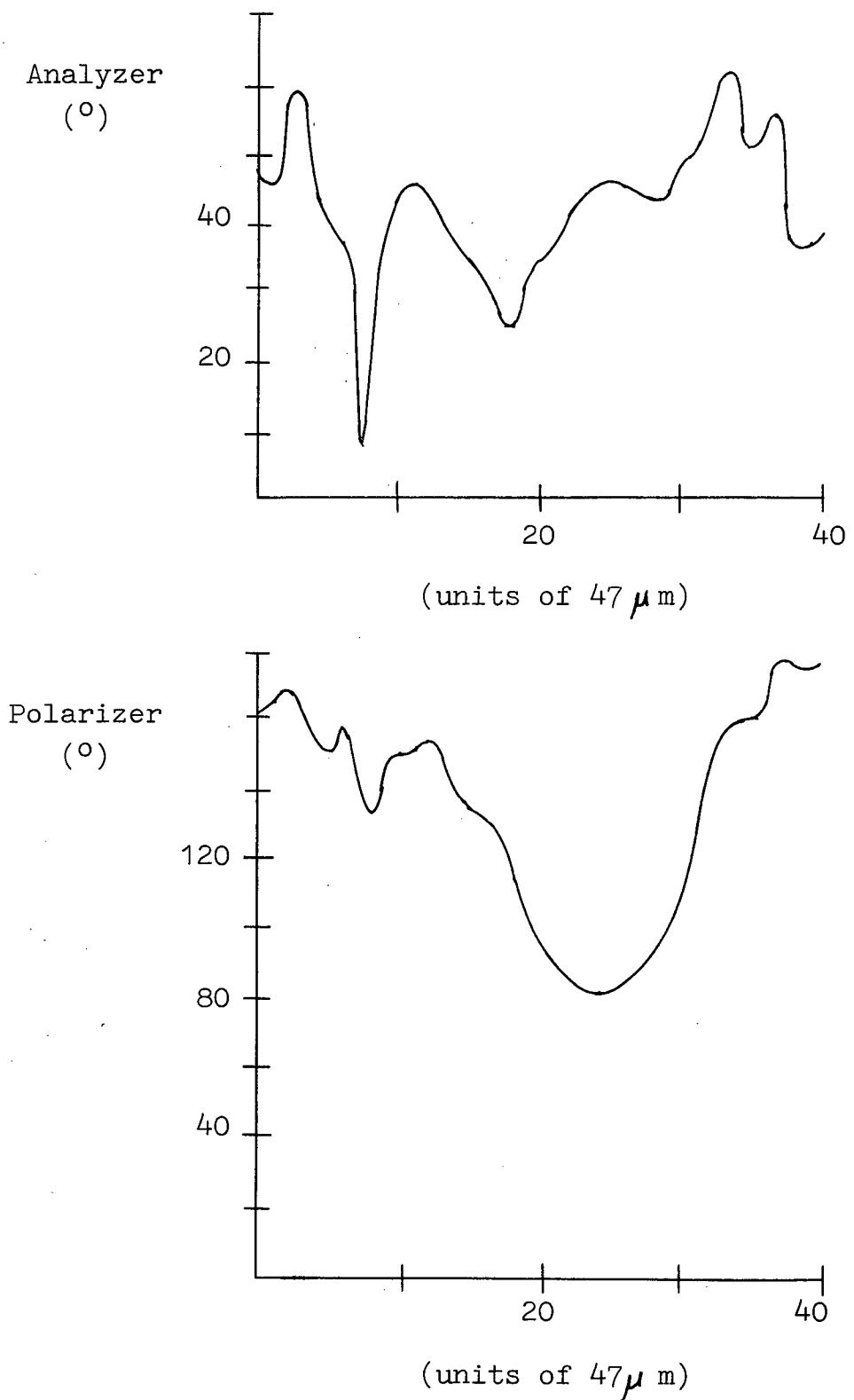


Figure 9. Polarizer and Analyzer Scan of Square 4

evaporation current was turned on, the control tape was read into the computer and the computer was allowed to control the evaporation and movements of the x-y holder. The photomultiplier reading was observed while the process was taking place.

The control system successfully found a null on the first square deposited, halted deposition and went on to the next square. On the second square, the null was very shallow and two shallow nulls were bypassed before manual intervention caused the process to proceed to the third and fourth squares. The control system again successfully detected nulls on these two areas and halted evaporation.

After the fourth square, the evaporation current was turned off and the ellipsometer was used to scan the center line of the four squares taking readings at short intervals. The scan is graphically presented in Figures 10 and 11. Finally, the holder was moved to a bare area and with the shutter open, continuous ellipsometer readings were taken. The $\Delta-\Psi$ curve from this data was plotted in Figure 12.

Using the average values of polarizer and analyzer readings from Table 2, the optical constants of the aluminum substrate, as viewed through the windows on the chamber, were determined using McCracken's program.¹¹ Using values for the index of zinc sulfide, the $\Delta-\Psi$ curve for the filter was calculated again using McCracken's program. This curve is presented graphically in Figure 13.

The scan of the bare aluminum substrate indicated that

Analyzer
($^{\circ}$)

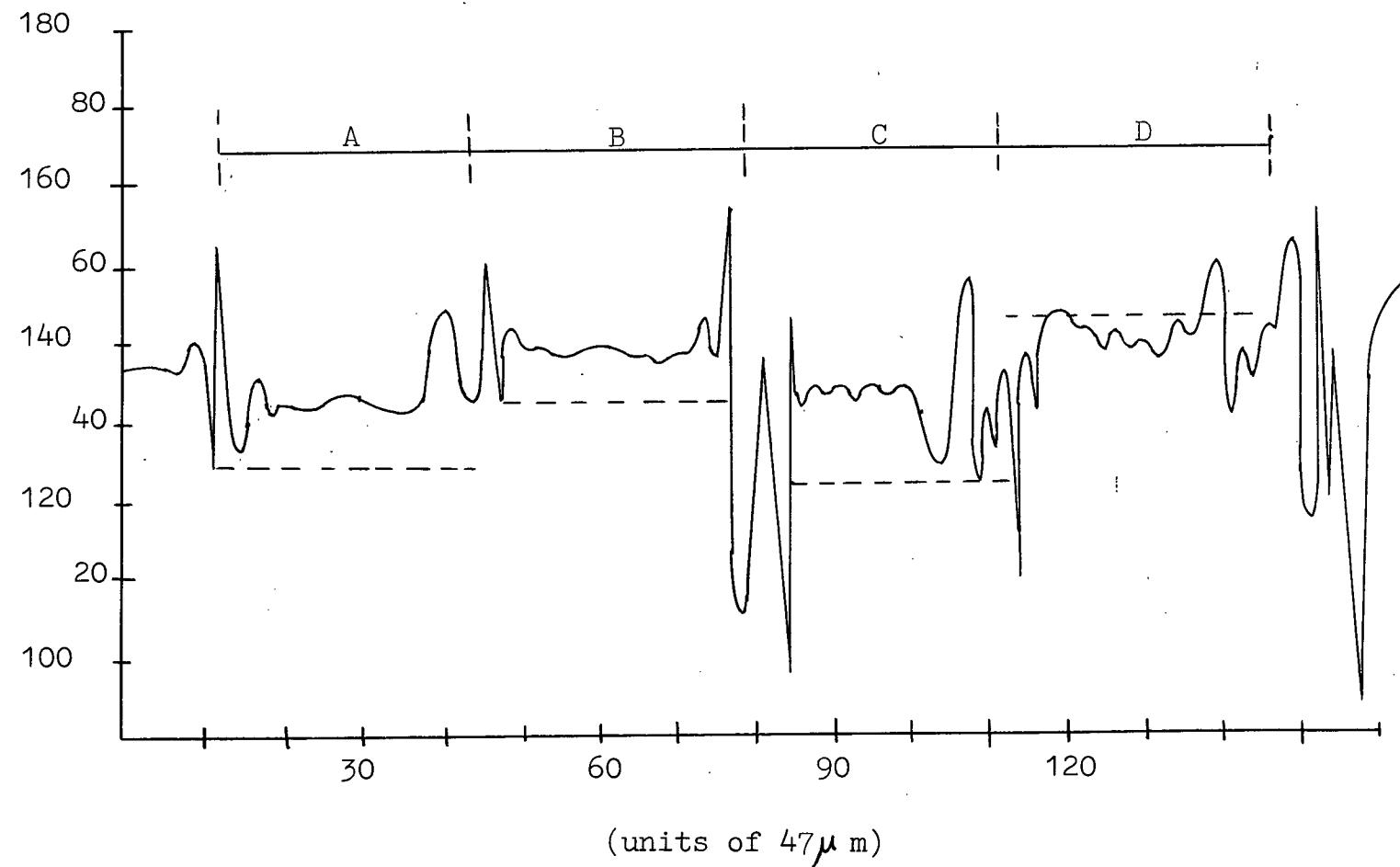


Figure 10. Analyzer Scan for Squares Deposited While on Control

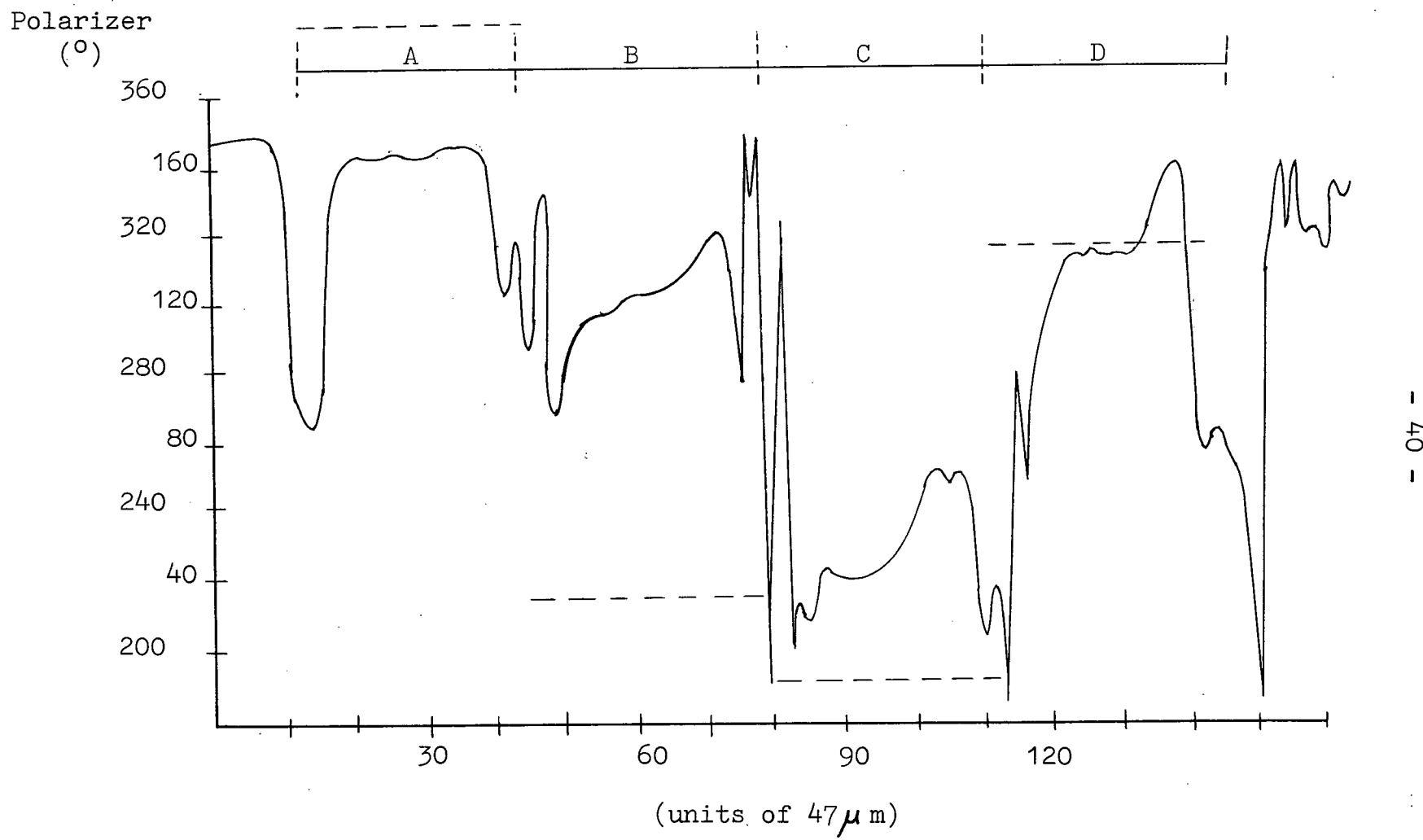


Figure 11. Polarizer Scan for Squares Deposited While on Control

the surface was uniform to an equivalent thickness of 20 angstroms of zinc sulfide as judged from the Δ - Ψ curve of Figure 13. The Δ and Ψ readings for the aluminum covered substrate, however, do not fit on the calculated curve for zinc sulfide on aluminum. The reason for this is probably that the "bare" aluminum is not really bare but has a coating of aluminum oxide which forms when aluminum is exposed to air. Therefore, the ellipsometer is actually measuring the aluminum and aluminum oxide layer as the substrate.

The results of the first experiment indicate mixed conclusions. The ellipsometer scan of the deposited squares point to nonuniform depositions and this was confirmed by visual examination of the substrate. The squares labelled 2 and 4 in Figures 7, 8 and 9 were uneven. The scan does, however, show clearly the definition of the squares. The edges of the square are defined by drastic changes in ellipsometer readings and the center sections are reasonably smooth.

The ellipsometer curve drawn from the measurements of the second experiment, Figure 12, differs from the theoretical curve for zinc sulfide on aluminum, Figure 13. Again, the most probable cause for this is the coating of aluminum oxide on the bare substrate. The index of vacuum deposited zinc sulfide films has been discovered to depend on the details of deposition such as rate of deposition, temperature and pressure.⁸ These findings could also contribute to the difference.

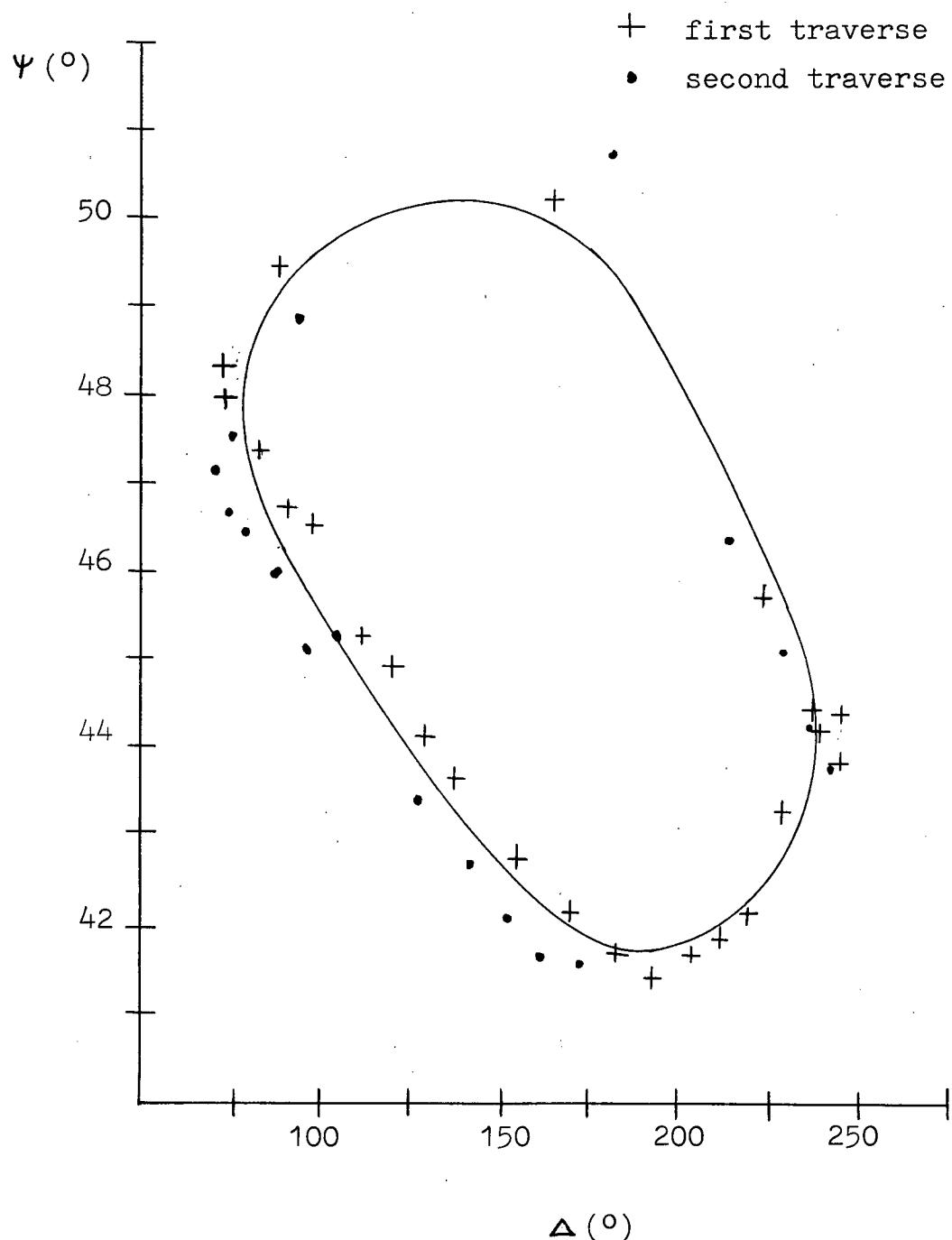


Figure 12. Δ - Ψ Plot (Experimental)

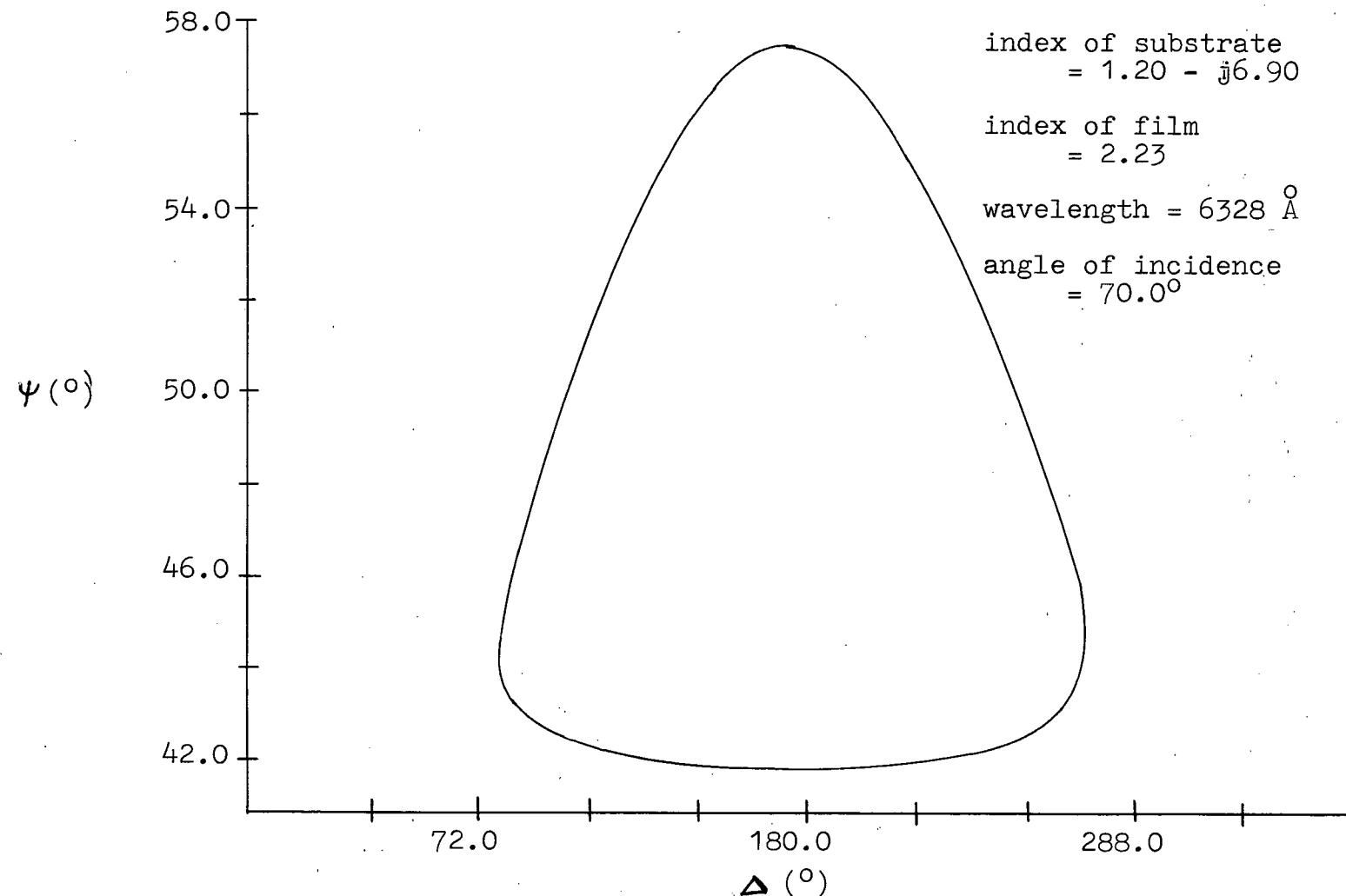


Figure 13. Δ - Ψ Plot (Calculated)

The computer control of thickness was successful to a limited extent. The actual control mechanism and algorithm performed well. The shutter was automatically closed to stop deposition after just passing the low point of a minimum from the ellipsometer readings. A poor selection process caused values of polarizer and analyzer readings to be chosen as setpoints. The chosen readings did not fall on the curve of Figure 12. The poor setpoints were evidenced by the shallow minimum in the ellipsometer output. The control system stopped deposition when it came as close as possible to the setpoints. During the deposition of the square labelled "D" in Figures 10 and 11, a sharp minimum was observed and as seen from later analysis, the control system came very close to the desired setpoints. The setpoints are shown as dotted straight lines in Figures 10 and 11.

The equipment built and experiments made have only tested the feasibility of producing phase filters with vacuum deposition techniques. To produce useful devices, the spatial resolution of the deposition system must be increased by an order of magnitude. This involves smaller apertures and closer tolerances on the positioning mechanisms. The experiments conducted have shown that the resolution used is attainable. The deposition system must be calibrated and errors introduced by the surface condition of the substrate must be accounted for. During the tests of this thesis, these factors were ignored as only relative

thickness of deposit was aimed for. The control and measurement systems seem capable of the tasks required of them. Thus, if further tests to calibrate the system were made, absolute thickness variations should be achievable.

In summary, a method of fabricating optical phase filters has been investigated. Possible uses of an optical phase filter have been proposed. The hardware to fabricate such a phase filter using vacuum deposition techniques was designed and constructed. Software was written to control production of the phase filters by a digital computer. And finally, the first steps were taken to produce the devices. The difficulties encountered were not fundamental in nature and require only refinements in technique to solve.

REFERENCES AND BIBLIOGRAPHY

1. Goodman, J.W.: Introduction to Fourier Optics, p. 80, McGraw Hill, New York, 1968.
2. Tsujiuchi, J.: "Correction of Optical Images by Compensation of Aberrations and by Spatial Frequency Filtering", Progress in Optics, Volume 2:133 (1963).
3. Ibid, pp. 145-149.
4. Upatnieko, J., A. Vander Lugt and E. Leith: "Correction of Lens Aberrations by Means of Holograms", Journal of Applied Optics, Volume 5:589 (1966).
5. Ibid, p. 590.
6. Lesem, L.B., P.M. Hirsh, and J.A. Jordan Jr.: IBM Journal of Residential Development, Volume 13:150 (1969).
7. McCabe, L., and J. Metals: AIME Transactions, Volume 200:969 (1954).
8. Rood, J.L.: "Evaporated Zinc Sulfide Films", Journal of the Optical Society of America, Volume 41:201 (1951).
9. Hall, J.F., and W.F.C. Ferguson: "Optical Properties of Cadmium Sulfide and Zinc Sulfide from 0.6 Micron to 14 Microns", Journal of the Optical Society of America, Volume 45:714 (1955).
10. Holland, L., and Steckelmacher, W.: Vacuum, Volume 2:346 (1952).
11. McCrackin, F.L.: A Fortran Program for Analysis of Ellipsometer Measurements, N.B.S. TN479, 1969.
12. McCrackin, F.L., Passaglia, E., Stromberg, R.R., and Steinberg, H.L.: Journal of Research of the National Bureau of Standards, 67A (1963).

APPENDIX I

A Program to Calculate Phase Changes Produced
by Varying Thickness

27 JAN. 76 00:00 DCO SCRC - FORTRAN COMPILER

```
1 C
2 C      TO CALCULATE REFLECTION COEFFICIENT OF FOLLOWING SYSTEM
3 C
4 C      *      *      */
5 C      *      *      */
6 C      *-----*      */
7 C      * NO      *-----*/
8 C      *          * N1      */
9 C      * DO      *      */
10 C     *          * D1      */   N2
11 C     *          *      */
12 C     *          *      */
13 C
14 C     ZO          Z1
15 C
16 C
17 COMPLEX CTHETA, CTHET1, CTHET2, DPO, DP1, R01P, R01S, R12P, R12S
18 COMPLEX NO, N1, N2, PHI, R1, R2, R3, REF, CEXP, CMPLX
19 C
20 C
21 C      INPUT PARAMETERS D=71-70 A FIXED DISTANCE
22 C          NO, N1, N2  REFRACTIVE INDICIES
23 C          WL        WAVELENGTH OF LIGHT
24 C          DINC     INCREMENT AT WHICH TO .CAL REFL COEF
25 C
26 READ(5,1) NO,N1,N2,D,DINC,WL
27 1 FORMAT(9E8.0)
28 C
29 C
30 C      PRINT OUT CONSTANTS
31 C
32 WRITE(6,2) NO,N1,N2,WL
33 2 FORMAT(1H1/,10X,6HN0 = (,F5.2,1H,,F5.2,1H),
34 1      /10X,6HN1 = (,F5.2,1H,,F5.2,1H),
35 2      /10X,6HN2 = (,F5.2,1H,,F5.2,1H),
36 3      //10X,12HWAVELENGTH = ,F6.0,9HANGSTROMS,
37 4      //5X,9HTHICKNESS,10X,12HPHASE CHANGE,
38 5      /5X,11H(ANGSTROMS),9X,9H(DEGREES)/)
39 C
40 C
41 PI=3.14159265
42 C
43 C      INITIALIZE VARIABLES
44 C
45 D1=0.
46 CTHETA=CMPLX(COS(0.),0.)
47 C
48 C
49 C      CALCULATE FRESENEL COEFFICIENTS
50 C
51 CALL REFL(NO,N1,CTHETA,CTHET1,R01P,R01S)
52 CALL REFL(N1,N2,CTHET1,CTHET2,R12P,R12S)
53 C
54 C
55 C      CALCULATE DO
56 C
57 3 DO=D-D1
```

27 JAN. 76 00:00 DCO SCRC - FORTRAN COMPILER

```
58 C
59 C
60 C      CALCULATE OPTICAL PATH LENGTHS
61 C
62      DPO=2.*DO*PI*N0*CTHETA/WL
63      DP1=2.*PI*D1*N1*CTHET1/WL
64 C
65 C
66 C      CALCULATE REFLECTION COEFFICIENT
67 C
68      R1=1.+R01P+R12P+R01P*R12P
69      R2=R01P+R12P*CEXP(DP1*CMPLX(0.,-2.))
70      R3=1.+R01P*R12P*CEXP(DP1*CMPLX(0.,-2.))
71      REF=(R1*R2/R3)*CEXP(DPO*CMPLX(0.,-2.))
72 C
73 C      CALCULATE PHASE OF REFLECTION COEFFICEINT
74 C
75 C      ANGLE=ATAN2(AIMAG(REF),REAL(REF))*180./PI
76      IF(ANGLE.LT.0.) ANGLE=ANGLE+360.
77 C
78 C      PRINT RESULTS
79 C
80 C      WRITE(6,4) D1,ANGLE
81 C      4 FORMAT(5X,F10.0,8X,F10.2)
82 C
83 C      INCREMENT D1 AND DO CALULATIONS AGAIN
84 C
85 C
86 C      D1=D1+DINC
87 C      IF(D1.LE.D) GO TO 3
88 C      CALL EXIT
89 C
90 C
91 END
```

27 JAN. 76 00:00 DCO SCRC - FORTRAN COMPILER

```
92 C
93 C      A SUBROUTINE TO CALCULATE THE PERPENDICULAR AND PARALLEL FRESNEL
94 C      REFLECTION COEFFICIENTS AT A BOUNDARY
95 C
96 C      INPUT PARAMETERS
97 C
98 C      N1,N2    INDICES OF REFRACTION ON EITHER SIDE OF BOUNDARY
99 C      THETA   COSINE OF ANGLE OF INCIDENCE
100 C
101 C
102 C      OUTPUT PARAMETERS
103 C
104 C      PHI     COSINE OF ANGLE OF REFRACTION
105 C      RP      PERPENDICULAR REFLECTION COEFFICIENT
106 C      RS      PARALLEL REFLECTION COEFFICIENT
107 C
108 C
109 C
110 C      SUBROUTINE REFL(N1,N2,THETA,PHI,RP,RS)
111 C      COMPLEX N1,N2,THETA,RS,RP,CSQRT,SI,SR,PHI
112 C
113 C
114 C      CALCULATE SINE OF ANGLE OF INCIDENCE
115 C
116 C      SI=CSQRT(1.-THETA*THETA)
117 C
118 C
119 C      USE SNELL'S LAW TO CALCULATE SINE OF ANGLE OF REFRACTANCE
120 C
121 C      SR=N1*SI/N2
122 C
123 C
124 C      CALCULATE COSINE OF ANGLE OF REFRACTANCE
125 C
126 C      PHI=CSQRT(1.-SR*SR)
127 C
128 C
129 C      CALCULATE REFLECTION COEFFICIENTS
130 C
131 C      RP=(N1*PHI-N2*THETA)/(N1*PHI+N2*THETA)
132 C      RS=(N1*THETA-N2*PHI)/(N1*THETA+N2*PHI)
133 C
134 C
135 C      RETURN
136 C      END
```

N0 = (1.00, 0.00)

N1 = (2.23, 0.00)

N2 = (1.20, -6.90)

WAVELENGTH = 6238. ANGSTROMS

THICKNESS (ANGSTROMS)	PHASE CHANGE (DEGREES)
0.	356.70
20.	356.50
40.	356.23
60.	355.89
80.	355.46
100.	354.93
120.	354.29
140.	353.52
160.	352.61
180.	351.53
200.	350.27
220.	348.79
240.	347.08
260.	345.10
280.	342.82
300.	340.21
320.	337.22
340.	333.81
360.	329.93
380.	325.53
400.	320.57
420.	315.00
440.	308.80
460.	301.94
480.	294.44
500.	286.33
520.	277.71
540.	268.71
560.	259.47
580.	250.21
600.	241.10
620.	232.32
640.	224.02
660.	216.29
680.	209.19
700.	202.75
720.	196.95
740.	191.78
760.	187.18
780.	183.12
800.	179.54
820.	176.40
840.	173.65
860.	171.26
880.	169.17
900.	167.37
920.	165.81
940.	164.47
960.	163.33

0.	356.70
20.	356.50
40.	356.23
60.	355.89
80.	355.46
100.	354.93
120.	354.29
140.	353.52
160.	352.61
180.	351.53
200.	350.27
220.	348.79
240.	347.08
260.	345.10
280.	342.82
300.	340.21
320.	337.22
340.	333.81
360.	329.93
380.	325.53
400.	320.57
420.	315.00
440.	308.80
460.	301.94
480.	294.44
500.	286.33
520.	277.71
540.	268.71
560.	259.47
580.	250.21
600.	241.10
620.	232.32
640.	224.02
660.	216.29
680.	209.19
700.	202.75
720.	196.95
740.	191.78
760.	187.18
780.	183.12
800.	179.54
820.	176.40
840.	173.65
860.	171.26
880.	169.17
900.	167.37
920.	165.81
940.	164.47
960.	163.33

980.	162. 35
1000.	161. 53
1020.	160. 85
1040.	160. 28
1060.	159. 82
1080.	159. 45
1100.	159. 15
1120.	158. 93
1140.	158. 76
1160.	158. 65
1180.	158. 57
1200.	158. 52
1220.	158. 50
1240.	158. 50
1260.	158. 50
1280.	158. 50
1300.	158. 50
1320.	158. 48
1340.	158. 45
1360.	158. 38
1380.	158. 27
1400.	158. 12
1420.	157. 92
1440.	157. 65
1460.	157. 30
1480.	156. 86
1500.	156. 33
1520.	155. 68
1540.	154. 90
1560.	153. 98
1580.	152. 89
1600.	151. 61
1620.	150. 12
1640.	148. 39
1660.	146. 39
1680.	144. 09
1700.	141. 46
1720.	138. 44
1740.	135. 00
1760.	131. 08
1780.	126. 65
1800.	121. 65
1820.	116. 04
1840.	109. 79
1860.	102. 89
1880.	95. 34
1900.	87. 20
1920.	78. 55
1940.	69. 52
1960.	60. 28
1980.	51. 02
2000.	41. 93

APPENDIX II

A Program to Calculate Fourier Transform Twice

27 JAN. 76 00:04 DCO SCRC - FORTRAN COMPILER

```
1 C
2 C
3 C A PROGRAM TO CALCULATE A TWO DIMENSIONAL SPATIAL FOURIER
4 C TRANSFORM, NORMALIZE THE TRANSFORM, AND TAKE THE
5 C TRANSFORM A SECOND TIME.
6 C
7 C
8 DIMENSION NA(64) ,B(64,64),C(64),ND(2)
9 COMPLEX A(64,64),AAA(64,64),CMPLX
10 N=64
11 ND(1)=N
12 ND(2)=N
13 C
14 C
15 C DEFINE BRIGHT AREAS BY *, OTHERWISE BLANK.
16 C
17 C READ(6,104) BLANK, STAR
18 C
19 C
20 C INPUT A PATTERN (BRIGHT AREA = 8)
21 C
22 DO 1 I=1,64
23 READ(5,101) (NA(J),J=I,N)
24 101 FORMAT(64I1)
25 C
26 C
27 C INITIALIZE FIELD TO 0.
28 C
29 DO 1 J=1,N
30 A(I,J)=CMPLX(0.,0.)
31 C
32 C
33 C SET BRIGHT AREAS TO 1.
34 C
35 IF(NA(J).EQ.8) A(I,J)=CMPLX(1.,0.)
36 1 CONTINUE
37 C
38 C
39 C DO FIRST TRANSFORM. (EXTERNAL SUBROUTINE)
40 C
41 CALL FOUR2(A,ND,2,-1,+1)
42 AM1=0.
43 C
44 C
45 C CHANGE AXES FROM -180,180 TO 0,360
46 C
47 DO 10 I=1,N
48 K=I+32
49 IF(I.GT.32) K=I-32
50 DO 10 J=1,N
51 L=J+32
52 IF(J.GT.32) L=J-32
53 X=REAL(A(I,J))
54 Y=AIMAG(A(I,J))
55 Z=SQRT(X*X+Y*Y)
56 IF(Z.GT.AM1) AM1=Z
57 10 AAA(K,L)=A(I,J)
```

27 JAN. 76 00:04 DCO SCRC - F O R T R A N C O M P I L E R

```
58      A2=.02*AM1
59      DO 50 I=1,N
60      DO 50 J=1,N
61      C
62      C
63      C      MAKE ALL INTENSITIES 1.
64      C
65      X=REAL(AAA(I,J))
66      Y=AIMAG(AAA(I,J))
67      Z=SQRT(X*X+Y*Y)
68      IF(Z.EQ.0.) GO TO 49
69      AAA(I,J)=AAA(I,J)/Z
70      49      IF(Z.LT.A2) AAA(I,J)=1.
71      50      CONTINUE
72      C
73      C
74      C      DO SECOND TRANSFORM:
75      C
76      CALL FOUR2(AAA,ND,2,-1,+1)
77      AMAX=0.
78      DO 3 I=1,N
79      DO 3 J=1,N
80      A(I,J)=AAA(I,J)
81      C
82      C
83      C      DETERMINE PEAK OF INTENSITY
84      C
85      X=REAL(A(I,J))
86      Y=AIMAG(A(I,J))
87      B(I,J)=SQRT(X*X+Y*Y)
88      IF(B(I,J).GT.AMAX) AMAX=B(I,J)
89      3      CONTINUE
90      WRITE(6,103) AMAX
91      103     FORMAT(10X,E10.3)
92      C
93      C
94      C      SET A LEVEL
95      C
96      AA=.01*AMAX
97      104     FORMAT(2A1)
98      DO 4 I=1,N
99      DO 5 J=1,N
100     C
101     C
102     C      PRINT PICTURE MARKING ELEMENTS ABOVE LEVEL
103     C
104     C(J)=BLANK
105     IF(B(I,J).GT.AA) C(J)=STAR
106     5      CONTINUE
107     4      WRITE(6,105) (C(J),J=1,N)
108     105    FORMAT(2X,64A1)
109     STOP
110     END
```

APPENDIX III

Listing of the Software Written for the PDP-8e

0076	0100	0000	SHFTH,	0	/VARIABLES
0077	0101	0000	SHFTL,	0	
0100	0102	0000	DVML,	0	
0101	0103	0000	DVMH,	0	
0102	0104	0000	MSDIG,	0	
0103	0105	0000	DNUMB,	0	
0104	0106	0000	ASUML,	0	
0105	0107	0000	ASUMH,	0	
0106	0110	0000	DIR,	0	
0107	0111	0100	STKL,	100	
0110	0112	7700	STKLC,	-100	
0111	0113	0000	SUMH1,	0	
0112	0114	0000	SUMH2,	0	
0113	0115	0000	SUML1,	0	
0114	0116	0000	SUML2,	0	
0115	0117	0000	STPCNT,	0	
0116	0120	1177	STSTK,	1177	
0117	0121	0000	AL,	0	
0120	0122	0000	AH,	0	
0121	0123	0000	BL,	0	
0122	0124	0000	BH,	0	
0123	0125	0000	CL,	0	
0124	0126	0000	CH,	0	
0125	0127	0003	POLCD,	3	
0126	0130	4010	ANZCD,	4010	
0127	0131	0200	M2XCD,	200	
0130	0132	0040	M2YCD,	40	
0131	0133	0000	DECL,	0	
0132	0134	0000	DECH,	0	
0133	0135	0000	DESTL,	0	
0134	0136	0000	DESTH,	0	
0135			/		
0136			/		
0137			*200		
0140			/		
0141			/		
0142			/INTERRUPT SERVICE		
0143			/		
0144	0200	3370	INTSER,	DCA ACCUM	/SAVE AC
0145	0201	7004		RAL	
0146	0202	3371		DCA LINK	/SAVE LINK
0147	0203	7701		ACL	
0150	0204	3372		DCA MQSAVE	/SAVE MQ
0151	0205	6031		KSF	/KEYBOARD?
0152	0206	7410		SKP	
0153	0207	5302		JMP KYBRD	
0154	0210	6041		TSF	/TELETYPE?
0155	0211	7410		SKP	
0156	0212	5223		JMP TELTP	/IF NEITHER
0157	0213	7300	EXTINT,	CLA CLL	/THEN EXIT
0160	0214	1371		TAD LINK	
0161	0215	7110		CLL HAR	/RESTORE LINK
0162	0216	1372		TAD MQSAVE	
0163	0217	7421		MQL	/RESTORE MQ
0164	0220	1370		TAD ACCUM	/RESTORE AC
0165	0221	6001		ION	/TURN INT ON
0166	0222	5400		JMP I O	/RETURN
0167			/		
0170			/		
0171			/TELETYPE SERVICE		
0172			/		
0173	0223	1373	TELTP,	TAD TELCNT	/ARE THERE MORE
0174	0224	7450		SNA	/CHAR TO TYPE

0175	0225	5244	JMP CTHUP	/NO
0176	0226	7041	CIA	/YES
0177	0227	7001	IAC	
0200	0230	7041	CIA	/DECREMENT CHAR
0201	0231	3373	DCA TELCNT	/COUNTER
0202	0232	1012	TAD TYPEPT	/END OF BUFFER
0203	0233	7041	CIA	/AREA REACHED?
0204	0234	1362	TAD ENDBUF	
0205	0235	7640	SZA CLA	
0206	0236	5241	JMP NOTEND	/NO
0207	0237	1363	TAD STBUF	/YES, RESET TO
0210	0240	3012	DCA TYPEPT	/START
0211	0241	1412	NOTEND, TAD I TYPEPT	/GET CHAR FROM /BUFFER
0212				
0213	0242	6046	TLS	/TYPE IT
0214	0243	5213	JMP EXTINT	/EXIT
0215	0244	7201	CTHUP, CLA IAC	/NO MORE CHAR
0216	0245	3364	DCA TFLAG	/SET TFLAG
0217	0246	6042	TCF	/CLEAR TTY FLAG
0220				/TO STOP TTY
0221	0247	5213	JMP EXTINT	/EXIT
0222			/	
0223			/	
0224			/PUT CHAR IN BUFFER TO BE TYPED	
0225			/	
0226	0250	0000	BUFFER, 0	/CHAR IN AC
0227	0251	3411	DCA I BUFPT	/PUT CHAR IN BUFF
0230	0252	2373	ISZ TELCNT	/INCRE CHAR COUNT
0231	0253	1373	BUFLP1, TAD TELCNT	/CHECK FOR FULL
0232	0254	1363	TAD STBUF	/BUFFER. WAIT
0233	0255	7841	CIA	/IN LOOP UNTIL
0234	0256	1362	TAD ENDBUF	/THERE IS ROOM
0235	0257	7650	SNA CLA	
0236	0260	5253	JMP BUFLP1	
0237	0261	6002	IOF	/NOT FULL. TURN /OFF INT TO AVOID /COMPLICATIONS
0240				/CHECK FOR END /OF BUFFER AREA
0241				
0242	0262	1011	TAD BUFPT	/CHECK FOR END
0243	0263	7041	CIA	/OF BUFFER AREA
0244	0264	1362	TAD ENDBUF	
0245	0265	7640	SZA CLA	
0246	0266	5271	JMP NOTEDB	/NOT END
0247	0267	1363	TAD STBUF	/END - RESET TO
0250	0270	3011	DCA BUFPT	/START
0251	0271	1364	NOTEDB, TAD TFLAG	/TEST TFLAG
0252	0272	7640	SZA CLA	/FLAG UP - MUST
0253	0273	5276	JMP CLTFLG	/RESTART TTY
0254	0274	6001	ION	/NOT UP - CONTINUE
0255	0275	5650	JMP I BUFFER	/EXIT - AC CLEAR
0256	0276	3364	CLTFLG, DCA TFLAG	/CLEAR TFLAG
0257	0277	6040	SPF	/RESTART TTY BY /SETTING TTY FLAG
0260				/TO RAISE INT.
0261				/CONTINUE
0262	0300	6001	ION	/EXIT - AC CLEAR
0263	0301	5650	JMP I BUFFER	
0264			/	
0265			/	
0266			/KEYBOARD SERVICE	
0267			/	
0270	0302	6034	KYBRD, KRS	/READ KBD
0271	0303	3413	DCA I KYBDPT	/STORE
0272	0304	2374	ISZ KBDCNT	/INCRE CHAR COUNT
0273	0305	1013	TAD KYBDPT	/CHECK FOR END

0274	0306	7041	CIA	/OF BUFFER AREA
0275	0307	1365	TAD ENDKBF	/AND RESET IF
0276	0310	7640	SZA CLA	/AT END
0277	0311	5314	JMP KYNEND	
0300	0312	1366	TAD STKYBF	
0301	0313	3013	DCA KYBDPT	
0302	0314	1374	KYNEND,	TAD KBDCNT /TEST FOR FULL
0303	0315	1366	TAD STKYBF	/BUFFER
0304	0316	7041	CIA	
0305	0317	1365	TAD ENDKBF	
0306	0320	7650	SNA CLA	
0307	0321	5324	JMP SETKFL	/BUFFER FULL
0310	0322	6032	KCC	/NOT FULL - SET
0311				/READER RUN
0312	0323	5213	JMP EXTINT	/EXIT
0313	0324	7201	SETKFL,	CLA IAC /FULL - SET KYFLAG
0314	0325	3367	DCA KYFLAG	
0315	0326	6030	KCF	/CLEAR KBD FLAG
0316				/DO NOT SET READER
0317				/RUN
0320	0327	5213	JMP EXTINT	/EXIT
0321			/	
0322			/	
0323			/TO REMOVE A CHARACTER FROM KBD BUFFER	
0324			/	
0325	0330	0000	READS,	0
0326	0331	1374	TAD KBDCNT	/IF BUFFER IS
0327	0332	7650	SNA CLA	/EMPTY, WAIT FOR
0330	0333	5331	JMP -2	/SOME INPUT
0331	0334	6002	IOF	/INT OFF TO AVOID
0332				/COMPLICATIONS
0333	0335	7240	CLA CMA	/DECREMENT CHAR
0334	0336	1374	TAD KBDCNT	/COUNTER
0335	0337	3374	DCA KBDCNT	
0336	0340	1014	TAD READPT	/CHECK FOR END OF
0337	0341	7041	CIA	/BUFFER AND RESET
0340	0342	1365	TAD ENDKBF	/IF AT END
0341	0343	7640	SZA CLA	
0342	0344	5347	JMP KYND2	
0343	0345	1366	TAD STKYBF	
0344	0346	3014	DCA READPT	
0345	0347	1367	KYND2,	TAD KYFLAG /WAS READER
0346	0350	7640	SZA CLA	/STOPPED?
0347	0351	5355	JMP FLAGUP	/YES
0350	0352	1414	TAD I READPT	/NO - GET CHAR
0351	0353	6001	ION	/LEAVE IN AC
0352	0354	5730	JMP I READB	/EXIT
0353	0355	3367	FLAGUP,	DCA KYFLAG /CLEAR KYFLAG
0354	0356	6032	KCC	/RESTART READER
0355	0357	1414	TAD I READPT	/GET CHARACTER
0356	0360	6001	ION	/LEAVE IN AC
0357	0361	5730	JMP I READB	/EXIT
0360	0362	7177	ENDBUF,	7177 /END OF OUTPUT
0361				/BUFFER
0362	0363	6777	STBUF,	6777 /START OF OUTPUT
0363				/BUFFER
0364	0364	0000	TFLAG,	0
0365	0365	7377	ENDKBF,	7377 /END OF INPUT
0366				/BUFFER
0367	0366	7177	STKYBF,	7177 /START OF INPUT
0370				/BUFFER
0371	0367	0000	KYFLAG,	0
0372	0370	0000	ACCUM,	0

0373 0371 0000 LINK, 0
0374 0372 0000 MQSAVE, 0
0375 0373 0000 TELCNT, 0
0376 0374 0000 KBDCNT, 0
0377 /
0400 /
0401 *400
0402 /
0403 /
0404 /TO PRODUCE A CARRIAGE RETURN AND LINE
0405 /FEED
0406 /
0407 0400 0000 CRLF, 0
0410 0401 7200 CLA
0411 0402 1215 TAD K215 /CR CHAR
0412 0403 4454 JMS I ABUFF /TYPE IT
0413 0404 1214 TAD K212 /LF CHAR
0414 0405 4454 JMS I ABUFF /TYPE IT
0415 0406 5600 JMP I CRLF /EXIT - AC CLEAR
0416 /
0417 /
0420 /TO PRODUCE A SPACE
0421 /
0422 0407 0000 SPACE, 0
0423 0410 7200 CLA
0424 0411 1216 TAD K240 /SPACE CHAR
0425 0412 4454 JMS I ABUFF /TYPE IT
0426 0413 5607 JMP I SPACE /EXIT - AC CLEAR
0427 /
0430 0414 0212 K212, 212
0431 0415 0215 K215, 215
0432 0416 0240 K240, 240
0433 /
0434 /
0435 /TO UNPACK A WORD AND PRINT IT OUT
0436 /SIMILAR TO PRINT PROGRAM IN DEC MANUAL
0437 /
0440 0417 0000 PRINT, 0
0441 0420 7300 CLA CLL
0442 0421 3301 DCA STNBR
0443 0422 1300 TAD NUMBER
0444 0423 7004 RAL
0445 0424 3301 DCA STNBR
0446 0425 1274 UNPACK, TAD ROTNBR
0447 0426 3305 DCA STROT
0450 0427 1301 TAD STNBR
0451 0430 7004 RAL
0452 0431 2305 ISZ STROT
0453 0432 5230 JMP .-2
0454 0433 3301 DCA STNBR
0455 0434 7004 RAL
0456 0435 3374 DCA LKPRT
0457 0436 1301 TAD STNBR
0460 0437 0273 AND MASK
0461 0440 1276 TAD K260
0462 0441 4454 JMS I ABUFF
0463 0442 1374 TAD LKPRT
0464 0443 7110 CLL RAR
0465 0444 2302 ISZ DIGCTR
0466 0445 5225 JMP UNPACK
0467 0446 5617 JMP I PRINT
0470 /

0472 /TO PRINT THE NUMBER IN THE AC AS A 3
0473 /DIGIT BCD NUMBER
0474 /
0475 0447 0000 PRTDC, 0 /
0476 0450 3300 DCA NUMBER /STORE
0477 0451 1303 TAD KC3 /SET NO OF DIGITS
0500 0452 3302 DCA DIGCTR /TO 3
0501 0453 1277 TAD KC4 /SET NO OF BITS
0502 0454 3274 DCA ROTNBR /PER DIGIT TO 4
0503 0455 1304 TAD MASK17 /SET UP 4 BIT MASK
0504 0456 3273 DCA MASK /
0505 0457 4217 JMS PRINT /USE PRINT
0506 0460 5647 JMP I PRTDC /EXIT - AC CLEAR
0507 /
0510 /
0511 /TO PRINT THE NUMBER IN THE AC AS A
0512 /4 DIGIT OCTAL NUMBER
0513 /
0514 0461 0000 PRTOC, 0 /
0515 0462 3300 DCA NUMBER /STORE NUMBER
0516 0463 1277 TAD KC4 /SET NO OF DIGITS
0517 0464 3302 DCA DIGCTR /TO 4
0520 0465 1303 TAD KC3 /SET NO OF BITS
0521 0466 3274 DCA ROTNBR /PER DIGIT TO 3
0522 0467 1275 TAD MASK7 /SET UP A 3 BIT
0523 0470 3273 DCA MASK /MASK
0524 0471 4217 JMS PRINT /USE PRINT
0525 0472 5661 JMP I PRTOC /EXIT - AC CLEAR
0526 /
0527 0473 0000 MASK, 0 /
0530 0474 0000 ROTNBR, 0 /
0531 0475 0007 MASK7, 7 /
0532 0476 0260 K260, 260 /
0533 0477 7774 KC4, -4 /
0534 0500 0000 NUMBER, 0 /
0535 0501 0000 STNBR, 0 /
0536 0502 0000 DIGCTR, 0 /
0537 0503 7775 KC3, -3 /
0540 0504 0017 MASK17, 17 /
0541 0505 0000 STROT, 0 /
0542 /
0543 /
0544 /TO READ THE ANALOG CHANNEL WHOSE CODE
0545 /IS IN THE AC
0546 /
0547 0506 0000 ANALG, 0 /
0550 0507 6323 6323 /CHANNEL SELECT
0551 0510 6321 6321 /WAIT FOR FLAG
0552 0511 5310 JMP .-1 /
0553 0512 7300 CLA CLL /
0554 0513 6324 6324 /READ
0555 0514 7040 CMA /INPUT IN OPPOSITE
0556 /LOGIC
0557 0515 4453 JMS I AMULT5 /MULT BY 5
0560 0516 7421 MQL /
0561 0517 7701 ACL /SPLIT RESULT INTO
0562 0520 0340 AND MK7700 /2 WORDS
0563 0521 7012 RTR /
0564 0522 7012 RTR /DIVIDE HIGH WORD
0565 0523 7012 RTR /BY 64
0566 0524 4453 JMS I AMULT5 /
0567 0525 4453 JMS I AMULT5 /MULT BY 25
0570 0526 3342 DCA SHIGH /STORE

0571 0527 7701 ACL
0572 0530 0341 AND MK77 /GET LOW HALF
0573 0531 4453 JMS I AMULT5
0574 0532 4453 JMS I AMULT5 /MULT BY 25
0575 0533 0340 AND MK7700 /DIVIDE LOW HALF
0576 0534 7002 BSW /BY 64
0577 0535 1342 TAD SHIGH /PUT HALVES BACK
0600 0536 7010 RAR /DIVIDE BY 2
0601 / /RESULT IS TO
0602 / /MULTBY (1000/1024)
0603 0537 5706 JMP I ANALG /EXIT - RESULT
0604 / /LEFT IN AC
0605 0540 7700 MK7700, 7700
0606 0541 0077 MK77, 77
0607 0542 0000 SHIGH, 0
0610 /
0611 /
0612 / TO INITILIZE THE POINTERS AND FLAGS
0613 /FOR THE OPERATING SYSTEM
0614 /
0615 0543 0000 INITZE, 0
0616 0544 7200 CLA
0617 0545 1366 TAD KK1777 /INITILIZE
0620 0546 3011 DCA BUFPT /POINTERS
0621 0547 1366 TAD KK1777
0622 0550 3012 DCA TYPEPT
0623 0551 1367 TAD KK2177
0624 0552 3013 DCA KYBDPT
0625 0553 1367 TAD KK2177
0626 0554 3014 DCA READPT
0627 0555 7201 CLA IAC
0630 0556 3770 DCA I ATFLAG /SET FLAGS
0631 0557 7201 CLA IAC
0632 0560 3771 DCA I AKFLAG
0633 0561 3773 DCA I ATLCNT /CLEAR COUNTERS
0634 0562 3772 DCA I AKYCNT
0635 0563 6032 KCC
0636 0564 6001 ION /TURN INTERRUPT ON
0637 0565 5743 JMP I INITZE /EXIT - AC CLEAR
0640 /
0641 0566 6777 KK1777, 6777
0642 0567 7177 KK2177, 7177
0643 0570 0364 ATFLAG, TFLAG
0644 0571 0367 AKFLAG, KYFLAG
0645 0572 0374 AKYCNT, KBDCT
0646 0573 0373 ATLCNT, TELCNT
0647 0574 0000 LKPRT, 0
0650 /
0651 /
0652 *600
0653 /
0654 /
0655 /PUT OUT PULSE TO STEP MOTORS
0656 /
0657 0600 0000 STEP1, 0
0660 0601 6334 6334 /PULSE TO STEP
0661 0602 7200 CLA
0662 0603 1210 TAD WT /WAIT LOOP
0663 0604 7001 IAC
0664 0605 7440 SZA
0665 0606 5204 JMP .-2
0666 0607 5600 JMP I STEP1 /EXIT - AC CLEAR
0667 0610 6500 WT, 6500 /DELAY FOR A RATE

0670 / OF 400 STEPS/SEC
0671 /
0672 /
0673 0611 0000 WAIT, 0
0674 0612 3225 DCA ENDTIM
0675 0613 6342 6342
0676 0614 6341 WLP1, 6341
0677 0615 5214 JMP --1
0700 0616 6344 6344
0701 0617 7040 CMA
0702 0620 7041 CIA
0703 0621 1225 TAD ENDTIM
0704 0622 7440 SZA
0705 0623 5214 JMP WLP1
0706 0624 5611 JMP I WAIT
0707 0625 0000 ENDTIM, 0
0710 /
0711 /
0712 /READ SHAFT ENCODER
0713 /
0714 0626 0000 RDSFT, 0
0715 0627 7200 CLA
0716 0630 6302 6302 /READ AND STORE
0717 0631 3100 DCA SHFTH /2 MSD
0720 0632 6304 6304 /READ AND STORE
0721 0633 3101 DCA SHFTL /3 LSD
0722 0634 5626 JMP I RDSFT /EXIT - AC CLEAR
0723 /
0724 /
0725 /READ DIGITAL VOLT METER
0726 /
0727 0635 0000 RDDVM, 0
0730 0636 7300 CLA CLL
0731 0637 6311 6311 /READ HIGH WORD
0732 0640 0252 AND MASK40 /TEST FLAG IN
0733 0641 7440 SZA /BIT 6
0734 0642 5236 JMP --4 /WAIT FOR FLAG
0735 0643 7200 CLA /TO GO DOWN
0736 0644 6301 6301 /READ AND STORE
0737 0645 3102 DCA DVML /LOW WORD
0740 0646 6311 6311 /READ AND STORE
0741 0647 0253 AND MASK37 /HIGH WORD (ONLY
0742 0650 3103 DCA DVMH /1 BCD CHAR)
0743 0651 5635 JMP I RDDVM /EXIT - AC CLEAR
0744 0652 0040 MASK40, 40
0745 0653 0037 MASK37, 37
0746 /
0747 /
0750 /TO ACCELERATE MOTORS
0751 /
0752 0654 0000 STEP, 0
0753 0655 7200 CLA
0754 0656 1110 TAD DIR /CHECK ACCEL FLAG
0755 / (BIT 9 OF DIR)
0756 0657 0315 AND MSKD1
0757 0660 7640 SZA CLA
0760 0661 5267 JMP ACCST /FLAG=1, START
0761 /ACCELERATION
0762 0662 1316 TAD ACCSTP /FLAG=0, CONTINUE
0763 /ACCELERATION
0764 0663 7640 SZA CLA /CHECK FOR END
0765 /OF ACCEL
0766 0664 5302 JMP ACCNTU /NO - CONT ACCEL

0767	0665	4200	JMS STEP1	/YES - STEP MOTOR	
0770	0666	5654	JMP I STEP	/EXIT - AC CLEAR	
0771	0667	7001	ACCST,	IAC	/START ACCEL
0772	0670	7440		SZA	/LET MOTOR SETTLE
0773	0671	5267		JMP .-2	
0774	0672	1315		TAD MSKDI	
0775	0673	7040		CMA	
0776	0674	0110		AND DIR	/CLEAR FLAG IN
0777	0675	3110		DCA DIR	/DIR TO CONTINUE
1000					/ACCELERATION
1001	0676	1317		TAD SKC16	/SET NUMBER OF
1002	0677	3316		DCA ACCSTP	/STEPS IN ACCEL
1003	0700	1320		TAD WTI	/SET ORIGINAL
1004	0701	3321		DCA WTIME	/EXTRA DELAY
1005	0702	4200	ACCNTU,	JMS STEP1	/STEP MOTOR
1006	0703	1321		TAD WTIME	
1007	0704	1322		TAD ACTIME	/DECREASE EXTRA
1010	0705	3321		DCA WTIME	/DELAY TIME
1011	0706	1321		TAD WTIME	
1012	0707	7001		IAC	/WAIT EXTRA DELAY
1013	0710	7440		SZA	
1014	0711	5307		JMP .-2	
1015	0712	2316		ISZ ACCSTP	/INCREMENT ACCEL
1016					/COUNTER
1017	0713	5654		JMP I STEP	
1020	0714	5654		JMP I STEP	
1021	0715	1000	MSKDI,	1000	/EXIT - AC CLEAR
1022	0716	0000	ACCSTP,	0	/MASK FOR FLAG
1023	0717	7760	SKC16,	-20	/ACCEL STEP COUNT
1024					/NUMBER OF ACCEL
1025	0720	5700	WTI,	5700	/STEPS
1026					/ORIGINAL EXTRA
1027	0721	0000	WTIME,	0	/DELAY
1030	0722	0100	ACTIME,	100	/TEMP STORAGE
1031					/DECREASE IN DELAY
1032					/
1033					/TO COMPLIMENT ANALYZER READING BY 360.00
1034					/
1035	0723	0000	ANZCP,	0	
1036	0724	7200		CLA	
1037	0725	1101		TAD SHFTL	/CONVERT LSDS
1040	0726	4442		JMS I ADCBIN	/((SHFTL) TO BIN)
1041	0727	7041		CIA	
1042	0730	1345		TAD K1000D	/1000(DEC)-SHFTL
1043	0731	4441		JMS I ABNBCD	/CONVERT TO BCD
1044	0732	1105		TAD DNUMB	/PUT BCD RESULT
1045	0733	3101		DCA SHFTL	/BACK IN SHFTL
1046	0734	1100		TAD SHFTH	/CONVERT MSDS
1047	0735	4442		JMS I ADCBIN	/((SHFTH) TO BIN)
1050	0736	7041		CIA	
1051	0737	1104		TAD MSDIG	/35(DEC)+CARRY
1052	0740	1346		TAD K35D	/-SHFTH
1053	0741	4441		JMS I ABNBCD	/CONVERT TO BCD
1054	0742	1105		TAD DNUMB	/PUT BCD RESULT
1055	0743	3100		DCA SHFTH	/IN SHFTH
1056	0744	5723		JMP I ANZCP	/EXIT - AC CLEAR
1057	0745	1750	K1000D,	1750	/1000(DEC)
1060	0746	0043	K35D,	43	/35(DEC)
1061					/
1062					/
1063					*1000
1064					/
1065					/

1066 /CONVERT 3 DIGIT BCD IN AC TO BINARY
1067 /LEAVE RESULT IN AC
1070 /
1071 1000 0000 DCBIN, 0
1072 1001 7421 MQL /SAVE BCD NO.
1073 1002 7701 ACL
1074 1003 0225 AND MK17 /SEPARATE LSD
1075 1004 3224 DCA OCNBR /STORE AS BIN
1076 1005 7701 ACL
1077 1006 0226 AND MK360 /SEPARATE MIDDLE
1100 1007 7112 CLL RTR /DIGIT
1101 1010 7012 RTR /RIGHT JUSTIFY
1102 1011 4230 JMS MULT10 /MULT BY 10
1103 1012 1224 TAD OCNBR /ADD TO BIN NO.
1104 1013 3224 DCA OCNBR
1105 1014 7701 ACL
1106 1015 0227 AND MK7400 /SEPARATE MSD
1107 1016 7106 CLL RTL /RIGHT JUSTIFY
1110 1017 7006 RTL
1111 1020 7004 RAL
1112 1021 4244 JMS MLT100 /MULT BY 100
1113 1022 1224 TAD OCNBR /ADD TO BIN NO.
1114 1023 5600 JMP I DCBIN /EXIT - BIN IN AC
1115 1024 0000 OCNBR, 0 /STORAGE FOR BIN
1116 1025 0017 MK17, 17 /MASK FOR LSD
1117 1026 0360 MK360, 360 /MASK FOR MID DIG
1120 1027 7400 MK7400, 7400 /MASK FOR MSD
1121 /
1122 /
1123 /MULT NO. IN AC BY 10 - LEAVE RESULT IN AC
1124 /
1125 1030 0000 MULT10, 0
1126 1031 4234 JMS MULT5 /MULT BY 5
1127 1032 7104 CLL RAL /MULT BY 2
1130 1033 5630 JMP I -MULT10
1131 /
1132 /
1133 /MULT NO. IN AC BY 5 - LEAVE RESULT IN AC
1134 /
1135 1034 0000 MULT5, 0
1136 1035 3243 DCA MNBR /STORE NO.
1137 1036 1243 TAD MNBR
1140 1037 7104 CLL RAL /MULT BY 2
1141 1040 7104 CLL RAL /MULT BY 2
1142 1041 1243 TAD MNBR /ADD NO.
1143 1042 5634 JMP I MULT5 /IE 5X=2X+2X+X
1144 1043 0000 MNBR, 0 /TEMP STORAGE
1145 /
1146 /
1147 /MULT AC BY 100 - RESULT IN AC
1150 /
1151 1044 0000 MLT100, 0
1152 1045 4230 JMS MULT10 /MULT BY 10
1153 1046 4230 JMS MULT10 /MULT BY 10
1154 1047 5644 JMP I MLT100
1155 /
1156 /
1157 /CONVERT BIN NO. IN AC TO 4 DIGITS BCD
1160 /RESULT IN MSDIG (MOST SIG DIGIT) AND
1161 /DNUMB (DECIMAL NO.) - ON PAGE 0
1162 /
1163 1050 0000 BNBCD, 0
1164 1051 3342 DCA BNBR /STORE BIN

1165	1052	7100	CLL	
1166	1053	3104	DCA MSDIG	/CLEAR
1167	1054	1342	TAD BNBR	
1170	1055	1344	BNLP1,	TAD KC1000 /SUBT 1000 FROM
1171	1056	7500	SMA	/BIN NO.
1172	1057	5263	JMP BACK	/IF AC IS NOT NEG
1173	1060	7430	SZL	/OR LINK=0 THEN
1174	1061	5263	JMP BACK	/INCREMENT MSDIG
1175	1062	5266	JMP FINISH	/AND SUBT 1000
1176	1063	2104	BACK,	ISZ MSDIG /AGAIN
1177	1064	7100	CLL	
1200	1065	5255	JMP BNLP1	
1201	1066	3342	FINISH,	DCA BNBR /IF AC IS LT 0
1202	1067	1344	TAD KC1000	/AND L=1, THEN
1203	1070	7041	CIA	/HAVE SUBT 1000
1204	1071	1342	TAD BNBR	/ONCE TOO OFTEN
1205	1072	3342	DCA BNBR	/ADD 1000 BACK ON
1206				
1207	1073	7300	CLA CLL	
1210	1074	3343	DCA DIG	/CLEAR
1211	1075	1342	TAD BNBR	
1212	1076	1345	BNLP2,	TAD KC100 /SUBT 100 FROM BIN
1213	1077	7500	SMA	/IF AC IS NOT NEG
1214	1100	5302	JMP BK2	/THEN INCREMENT
1215	1101	5304	JMP FNH2	/DIG AND SUBT
1216	1102	2343	BK2,	ISZ DIG /AGAIN
1217	1103	5276	JMP BNLP2	
1220	1104	3342	FNH2,	DCA BNBR /AC IS NEG - SAVE
1221	1105	1343	TAD DIG	/PUT NO. OF SUBT
1222	1106	7106	CLL RTL	/IN MSD POSITION
1223	1107	7006	RTL	/OF DNUMB
1224	1110	3105	DCA DNUMB	
1225	1111	1345	TAD KC100	/ADD 100 BACK
1226	1112	7041	CIA	/TO BIN NO.
1227	1113	1342	TAD BNBR	
1230	1114	3342	DCA BNBR	
1231				
1232	1115	7300	CLA CLL	
1233	1116	3343	DCA DIG	/CLEAR
1234	1117	1342	TAD BNBR	
1235	1120	1346	BNLP3,	TAD KC10 /SUBT 10 FROM
1236	1121	7500	SMA	/BIN NO. IF
1237	1122	5324	JMP BK3	/AC IS NOT NEG
1240	1123	5326	JMP FNH3	/INCR DIG AND
1241	1124	2343	BK3,	ISZ DIG /SUBT AGAIN
1242	1125	5320	JMP BNLP3	
1243	1126	3342	FNH3,	DCA BNBR /AC IS NEG - SAVE
1244	1127	1343	TAD DIG	/PUT NO. OF SUBT
1245	1130	1105	TAD DNUMB	/IN MID DIG OF
1246	1131	7106	CLL RTL	/DNUMB
1247	1132	7006	RTL	
1250	1133	3105	DCA DNUMB	
1251	1134	1346	TAD KC10	/ADD 10 BACK TO
1252	1135	7041	CIA	/BIN NO.
1253	1136	1342	TAD BNBR	
1254	1137	1105	TAD DNUMB	/PART LEFT IS LSD
1255	1140	3105	DCA DNUMB	/OF DNUMB
1256	1141	5650	JMP I BNBCD	/EXIT - AC CLEAR
1257				/
1260	1142	0000	BNBR,	0 /STOR FOR BIN NO.
1261	1143	0000	DIG,	0 /STOR FOR DIG
1262	1144	6030	KC1000,	6030 /-1000
1263	1145	7634	KC100,	7634 /-100

1264 1146 7766 KC10, 7766 /-10
1265 /
1266 /
1267 *1300
1270 /
1271 /
1272 /TO STORE A SET OF READINGS IN A STACK
1273 /FIXED LENGTH STACK - LATEST ADDITION
1274 /REPLACES EARLIEST - INPUT IN AC -
1275 /OUTPUT LEFT IN AC
1276 /
1277 1300 0000 STACK, 0
1300 1301 3323 DCA SVSTK1 /SAVE ADDITION
1301 1302 1010 TAD ENDSTK
1302 1303 7041 CIA /CHECK FOR END OF
1303 1304 1111 TAD STKL /STACK AREA AND
1304 1305 1120 TAD STSTK /RESET TO START
1305 1306 7440 SZA /IF AT END
1306 1307 5312 JMP +3 /STACK AREA IS
1307 1310 1120 TAD STSTK /1200 TO 1277
1310 1311 3010 DCA ENDSTK
1311 1312 7200 CLA
1312 1313 1410 TAD I ENDSTK /REMOVE NO. FROM
1313 1314 3324 DCA SVSTK2 /STACK AND SAVE IT
1314 1315 1010 TAD ENDSTK
1315 1316 3325 DCA ENDSK1 /REPLACE IT WITH
1316 1317 1323 TAD SVSTK1 /INPUT THAT WAS
1317 1320 3725 DCA I ENDSK1 /IN AC
1320 1321 1324 TAD SVSTK2 /PUT NO. REMOVED
1321 1322 5700 JMP I STACK /IN AC - EXIT
1322 1323 0000 SVSTK1, 0
1323 1324 0000 SVSTK2, 0
1324 1325 0000 ENDSK1, 0
1325 /
1326 /
1327 /TO READ THE PHOTOMULTIPLIER STKL NUMBER
1330 /OF TIMES AND KEEP A RUNNING SUM OF THE
1331 /READINGS STORED IN 2 WORDS, ASUMH, ASUML
1332 /
1333 1326 0000 SUM, 0
1334 1327 7200 CLA
1335 1330 1111 TAD STKL /SET COUNTER
1336 1331 7041 CIA
1337 1332 3117 DCA STPCNT
1340 1333 3107 DCA ASUMH /CLEAR STORAGE
1341 1334 3106 DCA ASUML
1342 1335 4347 LPSUM, JMS RDPTO /READ PHOTOMULT.
1343 1336 7100 CLL
1344 1337 1106 TAD ASUML /ADD TO ASUML
1345 1340 7430 SZL /IF OVERFLOW
1346 1341 2107 ISZ ASUMH /INCRE ASUMH
1347 1342 3106 DCA ASUML /STORE SUM
1350 1343 4433 JMS I ASTEP /STEP MOTOR
1351 1344 2117 ISZ STPCNT /LOOP
1352 1345 5335 JMP LPSUM
1353 1346 5726 JMP I SUM /EXIT - AC CLEAR
1354 /
1355 /
1356 /TO READ PHOTOMULTIPLIER - RESULT LEFT
1357 /IN AC
1360 /
1361 1347 0000 RDPTO, 0
1362 1350 7200 CLA

1363	1351	1354	TAD PHTOCD	/SET PTM CODE
1364	1352	4431	JMS I AANALG	/USE ANALG
1365	1353	5747	JMP I RDPTO	/EXIT - RESUT IN
1366				/AC
1367	1354	0017	PHTOCD, 17	/CODE FOR PTM
1370				/ANALG CHANNEL
1371		/		
1372		/		
1373			*1400	
1374		/		
1375		/		
1376			/TO REVERSE ELLIPSOMETER MOTORS	
1377		/		
1400	1400	0000	REV, 0	
1401	1401	7200	CLA	
1402	1402	1110	TAD DIR	
1403	1403	0216	AND MSKDIR	/SEPARATE
1404				/DIRECTION BITS
1405	1404	7040	CMA	/COMPLIMENT DIR
1406				/BITS
1407	1405	0216	AND MSKDIR	
1410	1406	3220	DCA CHDIR	/STORE COMP DIR
1411				/BITS
1412	1407	1110	TAD DIR	
1413	1410	0217	AND MSKDR2	/CLEAR OLD DIR
1414				/BITS AND FLAG
1415	1411	1233	TAD FLGSET	/SET FLAG TO
1416				/ACCELERATE
1417	1412	1220	TAD CHDIR	/SET CHANGED DIR
1420				/BITS
1421	1413	6332	6332	/SET FLIP FLOPS
1422	1414	3110	DCA DIR	/RESTORE IN DIR
1423	1415	5600	JMP I REV	/EXIT - AC CLEAR
1424	1416	0005	MSKDIR, 5	/MASK FOR DIR
1425				/BITS
1426	1417	6772	MSKDR2, 6772	/TO CLEAR FLAG
1427				/AND DIR BITS
1430	1420	0000	CHDIR, 0	/TEMP STORAGE
1431		/		
1432		/		
1433			/TO SET ACCELERATION FLAG AND FLIP FLOPS	
1434			/FOR MOTORS	
1435		/		
1436	1421	0000	SETM, 0	
1437	1422	3234	DCA MOTOR	/CODE FOR MOTORS
1440				/WAS IN AC
1441				/STORE IT
1442	1423	1110	TAD DIR	
1443	1424	0232	AND MSKDR1	/DO NOT CHANGE
1444				/SWITCH FF
1445	1425	1233	TAD FLGSET	/SET FLAG TO
1446				/START ACCEL
1447	1426	1234	TAD MOTOR	/SET MOTOR
1450				/INFORMATION
1451	1427	6332	6332	/SET FLIP FLOPS
1452	1430	3110	DCA DIR	/STORE IN DIR
1453	1431	5621	JMP I SETM	/EXIT - AC CLEAR
1454	1432	2000	MSKDR1, 2000	/MASK FOR SWITCH
1455				/FLIP FLOP
1456	1433	1000	FLGSET, 1000	/TO SET FLAG
1457	1434	0000	MOTOR, 0	/TEMP STORAGE
1460		/		
1461		/		

1462 /TO RUN MOTORS NUMBER OF STEPS IN AC
1463 /
1464 1435 0000 MOVE, 0
1465 1436 7041 CIA /SET COUNTER
1466 1437 3117 DCA STPCNT
1467 1440 4433 JMS I ASTEP /STEP MOTORS
1470 1441 2117 ISZ STPCNT
1471 1442 5240 JMP -2 /LOOP
1472 1443 5635 JMP I MOVE /EXIT - AC CLEAR
1473 /
1474 /
1475 /COMPO, COMP1, COMP2, SET ADDRESSES FOR
1476 /THE JUMP IN CMPSM (FOR USE IN BAL ROUTINE)
1477 /
1500 1444 0125 COMPO, CL /IF SUM2 IS LESS
1501 1445 1307 TAD APOS1 /THAN SUM1 THEN GO
1502 1446 3305 DCA S2LTS1 /TO POS 1
1503 1447 1306 TAD APOS0 /OTHERWISE GO TO
1504 1450 3304 DCA S2GTS1 /POS 0
1505 1451 5266 JMP CMPSM
1506 /
1507 /
1510 1452 7200 COMP1, CLA /IF SUM2 IS LESS
1511 1453 1307 TAD APOS1 /THAN SUM1 THEN
1512 1454 3305 DCA S2LTS1 /GO TO POS 1
1513 1455 1310 TAD APOS2 /OTHERWISE GO TO
1514 1456 3304 DCA S2GTS1 /POS 2
1515 1457 5266 JMP CMPSM
1516 /
1517 /
1520 1460 7200 COMP2, CLA /IF SUM2 IS LESS
1521 1461 1311 TAD APOS3 /THAN SUM1 THEN
1522 1462 3305 DCA S2LTS1 /GO TO POS 3
1523 1463 1312 TAD APOS4 /OTHERWISE GO TO
1524 1464 3304 DCA S2GTS1 /POS 4
1525 1465 5266 JMP CMPSM
1526 /
1527 /
1530 1466 7200 CMPSM, CLA /TO PERFORM
1531 1467 1115 TAD SUML1 /SUM1-SUM2 IN
1532 1470 3121 DCA AL /DOUBLE PRECISION
1533 1471 1113 TAD SUMH1 /AND TEST RESULT
1534 1472 3122 DCA AH
1535 1473 1116 TAD SUML2
1536 1474 3123 DCA BL
1537 1475 1114 TAD SUMR2
1540 1476 3124 DCA BH
1541 1477 4447 JMS I ADPSUB /(A-B=C)
1542 1500 1126 TAD CH /TEST RESULT
1543 1501 7500 SMA
1544 1502 5705 JMP I S2LTS1 /SUM2 LT SUM1
1545 1503 5704 JMP I S2GTS1 /SUM2 GT SUM1
1546 1504 0000 S2GTS1, 0 /ADDRESS SET BY
1547 1505 0000 S2LTS1, 0 /COMP ROUTINES
1550 1506 1622 APOS0, POS0 /LIST OF
1551 1507 1625 APOS1, POS1 /ADDRESSES
1552 1510 1633 APOS2, POS2
1553 1511 1660 APOS3, POS3
1554 1512 1713 APOS4, POS4
1555 /
1556 /
1557 /TO FILL STACK ORIGINALLY AND KEEP A
1560 /SUM OF THE READINGS

1561 /
1562 1513 0000 STORE, 0
1563 1514 7200 CLA
1564 1515 1112 TAD STKLC /SET COUNTER
1565 1516 3117 DCA STPCNT
1566 1517 1120 TAD STSTK /SET START OF STACK
1567 1520 3010 DCA ENDSTK
1570 1521 3106 DCA ASUML /CLEAR
1571 1522 3107 DCA ASUMH
1572 1523 4445 STLP1, JMS I ARDPTO /READ PTM
1573 1524 7421 MQL /STORE
1574 1525 7701 ACL
1575 1526 3410 DCA I ENDSTK /STORE IN STACK
1576 1527 7701 ACL
1577 1530 7100 CLL
1600 1531 1106 TAD ASUML /ADD TO ASUML
1601 1532 3106 DCA ASUML
1602 1533 7430 SZL /INCRE ASUMH
1603 1534 2107 ISZ ASUMH /IF OVERFLOW
1604 1535 4433 JMS I ASTEP /STEP MOTOR
1605 1536 2117 ISZ STPCNT
1606 1537 5323 JMP STLP1 /LOOP
1607 1540 5713 JMP I STORE /EXIT - AC CLEAR
1610 /
1611 /
1612 /DOUBLE PRECISION ADD A+B=C
1613 /(FROM DEC MANUAL INTRODUCTION TO PROG)
1614 /
1615 1541 0000 DPADD, 0
1616 1542 7300 CLA CLL
1617 1543 1121 TAD AL
1620 1544 1123 TAD BL
1621 1545 3125 DCA CL
1622 1546 7004 RAL
1623 1547 1122 TAD AH
1624 1550 1124 TAD BH
1625 1551 3126 DCA CH
1626 1552 5741 JMP I DPADD /EXIT - AC CLEAR
1627 /
1630 /
1631 /DOUBLE PRECISION SUBTRACTION A-B=C
1632 /(FROM DEC INTRO. TO PROG.)
1633 /
1634 1553 0000 DPSUB, 0
1635 1554 7300 CLA CLL
1636 1555 1123 TAD BL
1637 1556 7041 CIA
1640 1557 1121 TAD AL
1641 1560 3125 DCA CL
1642 1561 7004 RAL
1643 1562 3371 DCA KPDPS
1644 1563 1124 TAD BH
1645 1564 7040 CMA
1646 1565 1122 TAD AH
1647 1566 1371 TAD KPDPS
1650 1567 3126 DCA CH
1651 1570 5753 JMP I DPSUB /EXIT - AC CLEAR
1652 1571 0000 KPDPS, 0
1653 /
1654 /
1655 *1600
1656 /
1657 /

1660 /TO BALANCE THE ELLIPSOMETER
1661 /
1662 1600 0000 BAL, 0 /SET FLAG TO
1663 1601 7201 CLA IAC /INDICATE START
1664 1602 3323 DCA BLFLAG /TAKE SET OF READS
1665 1603 4724 STBL, JMS I ASUM /CLEAR POSITION
1666 1604 3321 DCA POSCT /POINTER
1667
1670 1605 1107 TAD ASUMH /STORE READINGS
1671 1606 3113 DCA SUMH1 /IN SUM1 (HIGH
1672 1607 1106 TAD ASUML /AND LOW)
1673 1610 3115 DCA SUML1 /TAKE ANOTHER SET
1674 1611 4724 BALLP1, JMS I ASUM /OF READINGS AND
1675 1612 1107 TAD ASUMH /STORE IN SUM2
1676
1677 1613 3114 DCA SUMH2 /CHECK FLAG. A
1700 1614 1106 TAD ASUML /CLEAR FLAG
1701 1615 3116 DCA SUML2 /INDICATES THAT
1702 1616 1323 TAD BLFLAG /A MINIMUM IS
1703 1617 7440 SZA /BEING APPROACHED
1704
1705
1706
1707 1620 5727 JMP I ACOMP0 /COMPARE SUM1
1710 1621 5730 JMP I ACOMP1 /AND SUM2
1711 1622 4443 POS0, JMS I AREV /GOING AWAY FROM
1712 1623 3323 DCA BLFLAG /MIN. REV MOTORS
1713 1624 5203 JMP STBL /CLEAR FLAG. START
1714
1715 1625 7200 POS1, CLA /OVER AGAIN
1716 1626 1114 TAD SUMH2 /GOING TOWARD A MIN
1717 1627 3113 DCA SUMH1 /PUT SUM2 INTO
1720 1630 1116 TAD SUML2 /SUM1
1721 1631 3115 DCA SUML1 /RETURN TO TAKE
1722 1632 5211 JMP BALLP1 /SUM2 AGAIN
1723 1633 4724 POS2, JMS I ASUM /GOING AWAY FROM
1724
1725
1726
1727
1730
1731
1732 1634 4443 JMS I AREV /MIN AFTER HAVING
1733 1635 1106 TAD ASUML /PASSED THROUGH IT
1734 1636 3115 DCA SUML1 /TAKE A SET OF
1735 1637 1107 TAD ASUMH /READINGS TO BE
1736 1640 3113 DCA SUMH1 /USED FOR
1737 1641 1111 TAD STKL /COMPARISON
1740 1642 4444 JMS I AMOVE /REV MOTORS
1741 1643 1111 TAD STKL /STORE READINGS
1742 1644 4444 JMS I AMOVE /IN SUM1
1743 1645 4726 JMS I ASTORE /MOVE BACK TWO
1744 1646 7200 CLA /SETS OF READINGS
1745 1647 1107 TAD ASUMH /STORE NEXT SET
1746 1650 3114 DCA SUMH2 /OF READINGS IN
1747 1651 1106 TAD ASUML /STACK AND STORE
1750 1652 3116 DCA SUML2 /THE SUM IN SUM2
1751 1653 1111 TAD STKL /SET POSITION
1752 1654 1111 TAD STKL /POINTER TO NO.
1753 1655 1111 TAD STKL /OF STEPS TAKEN
1754 1656 3321 DCA POSCT /FROM COMPARISON
1755
1756 1657 5731 JMP I ACOMP2 /SUM
 /COMPARE SUM2 AND

1757				/SUM1	
1760	1660	7200	POS3,	CLA	/HAVE NOT YET
1761					/COME TO SAME
1762					/DISTANCE FROM MIN
1763					/AS COMPARISON SUM
1764	1661	2321		ISZ POSCT	/INCRE POS POINTER
1765	1662	4445		JMS I ARDPTO	/TAKE A SINGLE
1766					/READING
1767	1663	7421		MQL	
1770	1664	7701		ACL	/STORE IT IN STACK
1771	1665	4725		JMS I ASTACK	
1772	1666	3123		DCA BL	/SUBTRACT READING
1773	1667	3124		DCA BH	/REMOVED FROM STACK
1774	1670	7701		ACL	/FROM READING PUT
1775	1671	3121		DCA AL	/IN STACK
1776	1672	3122		DCA AH	
1777	1673	4447		JMS I ADPSUB	
2000	1674	1125		TAD CL	/ADD RESULT TO
2001	1675	3121		DCA AL	/SUM2
2002	1676	1126		TAD CH	
2003	1677	3122		DCA AH	
2004	1700	1116		TAD SUML2	
2005	1701	3123		DCA BL	
2006	1702	1114		TAD SUMH2	
2007	1703	3124		DCA BH	
2010	1704	4450		JMS I ADPADD	
2011	1705	1125		TAD CL	
2012	1706	3116		DCA SUML2	
2013	1707	1126		TAD CH	
2014	1710	3114		DCA SUMH2	
2015	1711	4433		JMS I ASTEP	/MOVE MOTOR ONE
2016					/STEP
2017	1712	5731		JMP I ACOMP2	/COMPARE SUM1
2020					/AND SUM2
2021					/IF SUM2 LT SUM1
2022					/RETURN TO POS3
2023	1713	4443	POS4,	JMS I AREV	/OTHERWISE HAVE
2024					/FOUND BALANCE
2025					/REVERSE MOTORS
2026	1714	7300		CLA CLL	/DRIVE TO MIDPOINT
2027	1715	1321		TAD POSCT	/OF SUM1 AND SUM2
2030	1716	7010		RAR	
2031	1717	4444		JMS I AMOVE	
2032	1720	5600		JMP I BAL	/EXIT - AC CLEAR
2033					/ELLIPSOMETER
2034					/UNIT LEFT AT
2035					/BALANCED POSITION
2036	1721	0000	POSCT,	0	/POSITION POINTER
2037	1722	0000	HLDLB1,	0	
2040	1723	0000	BLFLAG,	0	/BALANCE FLAG
2041	1724	1326	ASUM,	SUM	/ADDRESSES USED
2042	1725	1300	ASTACK,	STACK	/BY BAL ROUTINE
2043	1726	1513	ASTORE,	STORE	
2044	1727	1444	ACOMP0,	COMP0	
2045	1730	1452	ACOMP1,	COMP1	
2046	1731	1460	ACOMP2,	COMP2	
2047				/	
2050				/	
2051				*2000	
2052				/	
2053				/	
2054				/TO SET DESIRED UNIT OF ELLIPSOMETER	
2055				/TO A REQUIRED POSITION	

2056				
2057	2000	0000	SETEL, 0	
2060	2001	4435	JMS I ARDSFT	/READ SHAFT ENCODER
2061	2002	1365	TAD FWD	/TO DETERMINE POS
2062	2003	7184	CLL RAL	/OF UNIT
2063	2004	7630	SZL CLA	/DETERMINE WHETHER
2064				/ANZ OR POL IS TO
2065	2005	4451	JMS I AANZCP	/SET. IF ANZ
2066				/COMPLIMENT BY 360
2067	2006	1101	TAD SHFTL	
2070	2007	3133	DCA DECL	/CONVERT POSITION
2071	2010	1100	TAD SHFTH	/FROM BCD TO BINARY
2072	2011	3134	DCA DECH	
2073	2012	4457	JMS I ADPDBN	
2074	2013	1125	TAD CL	
2075	2014	3101	DCA SHFTL	/STORE POS IN
2076	2015	1126	TAD CH	/SHAFT(LOW,HIGH)
2077	2016	3100	DCA SHFTH	
2100	2017	1135	TAD DESTL	
2101	2020	3121	DCA AL	/PERFORM
2102	2021	1136	TAD DESTH	/((DEST-SHAFT))
2103	2022	3122	DCA AH	
2104	2023	1101	TAD SHFTL	
2105	2024	3123	DCA BL	
2106	2025	1100	TAD SHFTH	
2107	2026	3124	DCA BH	
2110	2027	4447	SUBPT, JMS I ADPSUB	/IS RESULT -VE,
2111	2030	1126	TAD CH	/0, OR +VE?
2112	2031	7640	SZA CLA	
2113	2032	5236	JMP .+4	
2114	2033	1125	TAD CL	
2115	2034	7650	SNA CLA	
2116	2035	5600	JMP I SETEL	/IF 0 THEN DONE
2117	2036	1126	TAD CH	
2120	2037	7700	SMA CLA	
2121	2040	5260	JMP AHEAD	/IF +VE JUMP
2122	2041	1135	TAD DESTL	
2123	2042	3123	DCA BL	/IF -VE INTER-
2124	2043	1136	TAD DESTH	/CHANGE DEST AND
2125	2044	3124	DCA BH	/SHAFT AND DIR
2126	2045	1101	TAD SHFTL	/CODES (FWD FOR-
2127	2046	3121	DCA AL	/BKD AND VICE
2130	2047	1100	TAD SHFTH	/VERSA)
2131	2050	3122	DCA AH	
2132	2051	1366	TAD BKWD	
2133	2052	3377	DCA BHLDK	
2134	2053	1365	TAD FWD	
2135	2054	3366	DCA BKWD	
2136	2055	1377	TAD BHLDK	
2137	2056	3365	DCA FWD	
2140	2057	5227	JMP SUBPT	/DO SUBT AGAIN
2141	2060	1126	AHEAD, TAD CH	
2142	2061	3372	DCA DMSEH	/STORE DEST-SHAFT
2143	2062	1125	TAD CL	/IN DMSE
2144	2063	3371	DCA DMSEL	
2145	2064	1126	TAD CH	
2146	2065	3122	DCA AH	/PERFORM
2147	2066	1125	TAD CL	/((DMSE-180.00))
2150	2067	3121	DCA AL	/TO DETERMINE
2151	2070	1373	TAD H180	/SHORTEST DIRECTION
2152	2071	3124	DCA BH	/TO TRAVEL
2153	2072	1374	TAD L180	
2154	2073	3123	DCA BL	

2155	2074	4447	JMS I ADPSUB	
2156	2075	1126	TAD CH	
2157	2076	7710	SPA CLA	
2160	2077	5326	JMP MVEFWD	/IF -VE OR 0
2161				/MOVE FORWARD
2162	2100	1375	TAD H360	/IF +VE
2163	2101	3122	DCA AH	/PERFORM
2164	2102	1376	TAD L360	((360.00-DMSE)
2165	2103	3121	DCA AL	
2166	2104	1372	TAD DMSEH	
2167	2105	3124	DCA BH	
2170	2106	1371	TAD DMSEL	
2171	2107	3123	DCA BL	
2172	2110	4447	JMS I ADPSUB	
2173	2111	1366	TAD BKWD	
2174	2112	4452	JMS I ASETM	/SET MOTORS TO
2175	2113	1126	TAD CH	/MOVE BACKWARDS
2176	2114	7450	SNA	/MOVE 10000(OCT)
2177	2115	5323	JMP .+6	/STEPS FOR EACH
2200	2116	7041	CIA	/COUNT IN CH
2201	2117	3126	DCA CH	
2202	2120	4444	JMS I AMOVE	
2203	2121	2126	ISZ CH	
2204	2122	5320	JMP .-2	
2205	2123	1125	TAD CL	/MOVE CL STEPS
2206	2124	4444	JMS I AMOVE	
2207	2125	5600	JMP I SETEL	/EXIT - AC CLEAR
2210	2126	1365	MVEFWD, TAD FWD	
2211	2127	4452	JMS I ASETM	/SET MOTORS TO
2212	2130	1372	TAD DMSEH	/MOVE FORWARD
2213	2131	7450	SNA	
2214	2132	5340	JMP .+6	/MOVE AS ABOVE
2215	2133	7041	CIA	
2216	2134	3372	DCA DMSEH	
2217	2135	4444	JMS I AMOVE	
2220	2136	2372	ISZ DMSEH	
2221	2137	5335	JMP .-2	
2222	2140	1371	TAD DMSEL	
2223	2141	4444	JMS I AMOVE	
2224	2142	5600	JMP I SETEL	
2225			/	
2226			/	
2227			/TO SET THE ANALYZER TO THE POSITION	
2230			/STORED IN DESTH, DESTL (A TWO WORD BINARY	
2231			/NUMBER IN THE RANGE 0 TO 35999 DECIMAL)/	
2232	2143	0000	SETAN, 0	
2233	2144	1130	TAD ANZCD	/GET ANZ CODE
2234	2145	4452	JMS I ASETM	/SET GATING
2235	2146	1130	TAD ANZCD	
2236	2147	3366	DCA BKWD	/SET FWD AND BKWD
2237	2150	1367	TAD ANZ2	/CODES TO BE USED
2240	2151	3365	DCA FWD	/BY SETEL
2241	2152	4200	JMS SETEL	
2242	2153	5743	JMP I SETAN	/EXIT - AC CLEAR
2243			/	
2244			/	
2245			/TO SET POLARIZER AS ABOVE	
2246			/	
2247	2154	0000	SETPL, 0	
2250	2155	1127	TAD POLCD	/GET POL CODE
2251	2156	4452	JMS I ASETM	
2252	2157	1127	TAD POLCD	/AS ABOVE
2253	2160	3365	DCA FWD	

2254 2161 1370 TAD POL2
2255 2162 3366 DCA BKWD
2256 2163 4200 JMS SETEL
2257 2164 5754 JMP I SETPL /EXIT - AC CLEAR
2260 /
2261 2165 0000 FWD, 0
2262 2166 0000 BKWD, 0
2263 2167 4014 ANZ2, 4014
2264 2170 0002 POL2, 2
2265 2171 0000 DMSEL, 0
2266 2172 0000 DMSEH, 0
2267 2173 0004 H180, 4
2270 2174 3120 L180, 3120
2271 2175 0010 H360, 10
2272 2176 6240 L360, 6240
2273 2177 0000 BHLDK, 0
2274 *2200 /
2275 /
2276 /
2277 /TO CONVERT A TWO WORD BCD NUMBER TO BINARY
2300 /BCD IN DECH, DECL BINARY IN CH, CL
2301 /
2302 2200 0000 DPDBN, 0
2303 2201 1134 TAD DECH /CONVERT HIGH
2304 2202 4442 JMS I ADCBIN /WORD TO BIN
2305 2203 3237 DCA DPX2L
2306 2204 3240 DCA DPX2H
2307 2205 4245 JMS DPX2
2310 2206 4245 JMS DPX2 /MULT BY 2X2X2=8
2311 2207 4245 JMS DPX2
2312 2210 1243 TAD CNT3 /SET UP TO MULT
2313 2211 3244 DCA CNT3HD /BY 5X5X5=125
2314 2212 1237 TAD DPX2L
2315 2213 3241 DCA DPX5L
2316 2214 1240 TAD DPX2H
2317 2215 3242 DCA DPX5H
2320 2216 4255 JMS DPX5 /MULT BY 5
2321 2217 1126 TAD CH
2322 2220 3242 DCA DPX5H /NET RESULT IS TO
2323 2221 1125 TAD CL /MULT DECH BY
2324 2222 3241 DCA DPX5L /1000(DECIMAL)
2325 2223 2244 ISZ CNT3HD
2326 2224 5216 JMP .-6
2327 2225 1125 TAD CL
2330 2226 3121 DCA AL
2331 2227 1126 TAD CH
2332 2230 3122 DCA AH
2333 2231 1133 TAD DECL /CONVERT DECL
2334 2232 4442 JMS I ADCBIN /TO BINARY
2335 2233 3123 DCA BL
2336 2234 3124 DCA BH /ADD TO HIGH PART
2337 2235 4450 JMS I ADPADD
2340 2236 5600 JMP I DPDBN /EXIT - AC CLEA
2341 2237 0000 DPX2L, 0
2342 2240 0000 DPX2H, 0
2343 2241 0000 DPX5L, 0
2344 2242 0000 DPX5H, 0
2345 2243 7775 CNT3, -3
2346 2244 0000 CNT3HD, 0
2347 /
2350 /
2351 /DOUBLE PRECISION MULTIPLY BY 2
2352 /INPUT AND OUTPUT IN DPX2H, DPM2L

2353
2354 2245 0000 DPX2, 0
2355 2246 1237 TAD DPX2L
2356 2247 7104 CLL RAL /ROTATE ONE LEFT
2357 2250 3237 DCA DPX2L
2360 2251 1240 TAD DPX2H
2361 2252 7004 RAL
2362 2253 3240 DCA DPX2H
2363 2254 5645 JMP I DPX2 /EXIT - AC CLEAR
2364 /
2365 /
2366 /DOUBLE PRECISION MULTIPLY BY 5
2367 /INPUT IN DPX5H, DPX5L OUTPUT IN CH, CL
2370 /
2371 2255 0000 DPX5, 0
2372 2256 1241 TAD DPX5L /SET UP TO X2
2373 2257 3237 DCA DPX2L
2374 2260 1242 TAD DPX5H
2375 2261 3240 DCA DPX2H
2376 2262 4245 JMS DPX2 /X2
2377 2263 4245 JMS DPX2 /X2
2400 2264 1237 TAD DPX2L
2401 2265 3121 DCA AL /ADD ON ORIGINAL
2402 2266 1240 TAD DPX2H /NUMBER
2403 2267 3122 DCA AH
2404 2270 1241 TAD DPX5L
2405 2271 3123 DCA BL
2406 2272 1242 TAD DPX5H
2407 2273 3124 DCA BH
2410 2274 4450 JMS I ADPADD
2411 2275 5655 JMP I DPX5 /EXIT - AC CLEAR
2412 /
2413 /
2414 /TO TURN ON POWER TRANSISTOR
2415 /
2416 2276 0000 ONSW, 0
2417 2277 7200 CLA
2420 2300 1110 TAD DIR /CLEAR BIT 1
2421 2301 0315 AND MK2000 /OF DIR
2422 2302 1316 TAD MC2000 /SET BIT 1 OF DIR
2423 2303 6332 6332 /SET GATES
2424 2304 3110 DCA DIR /STORE CHANGE
2425 2305 5676 JMP I ONSW /EXIT - AC CLEAR
2426 /
2427 /
2430 /TO TURN OFF POWER TRANSISTOR
2431 /
2432 2306 0000 OFFSW, 0
2433 2307 7200 CLA
2434 2310 1110 TAD DIR /CLEAR BIT 1
2435 2311 0315 AND MK2000 /OF DIR
2436 2312 6332 6332 /SET GATES
2437 2313 3110 DCA DIR /STORE CHANGE
2440 2314 5706 JMP I OFFSW /EXIT - AC CLEAR
2441 /
2442 2315 5777 MK2000, 5777
2443 2316 2000 MC2000, 2000
2444 /
2445 /
2446 *2400
2447 /
2450 /
2451 /TO BALANCE THE POLARIZER AND TYPE

2452 /OUT THE BALANCE POSITION
2453
2454 2400 0000 BALP, Ø
2455 2401 7200 CLA
2456 2402 1127 TAD POLCD /SET POL
2457 2403 4452 JMS I ASETM /CODE
2460 2404 4214 JMS BALU /USE BALU
2461 2405 5600 JMP I BALP /EXIT - AC CLEAR
2462
2463
2464 /TO BALANCE THE ANALYZER AND TYPE
2465 /OUT THE BALANCE POSITION
2466
2467 2406 0000 BALA, Ø
2470 2407 7200 CLA
2471 2410 1130 TAD ANZCD /SET ANZ
2472 2411 4452 JMS I ASETM /CODE
2473 2412 4214 JMS BALU /USE BALU
2474 2413 5606 JMP I BALA /EXIT - AC CLEAR
2475
2476
2477 /TO BALANCE THE UNIT SPECIFIED ABOVE
2500
2501 2414 0000 BALU, Ø
2502 2415 4432 JMS I ASPACE
2503 2416 4432 JMS I ASPACE /TYPE 2 SPACES
2504 2417 4446 JMS I ABAL /BALANCE
2505 2420 1247 TAD CH1CD /READ
2506 2421 4431 JMS I AANALG /PHOTOMULTIPLIER
2507 2422 3352 DCA ESIG /STORE READING
2510 2423 4435 JMS I ARDSFT /READ SHAFT ENCODER
2511 2424 1110 TAD DIR /IF ANZ THEN COMP
2512 2425 7104 CLL RAL /BY 360.00
2513 2426 7630 SZL CLA
2514 2427 4451 JMS I AANZCP
2515 2430 1100 TAD SHFTH /PRINT OUT
2516 2431 4440 JMS I APRTD
2517 2432 1101 TAD SHFTL /SHAFT ENCODER
2520 2433 4440 JMS I APRTD
2521 2434 4432 JMS I ASPACE
2522 2435 4432 JMS I ASPACE /PRINT 3 SPACES
2523 2436 4432 JMS I ASPACE
2524 2437 1250 TAD CE
2525 2440 4454 JMS I ABUFF /TYPE ESC(ERROR
2526 2441 1251 TAD CS /SIGNAL)
2527 2442 4454 JMS I ABUFF
2530 2443 4432 JMS I ASPACE /LEAVE SPACE
2531 2444 1352 TAD ESIG /PRINT OUT ES
2532 2445 4437 JMS I APRTOC
2533 2446 5614 JMP I BALU /EXIT - AC CLEAR
2534 2447 0017 CH1CD, 0017
2535 2450 0305 CE, 305
2536 2451 0323 CS, 323
2537
2540
2541 /TO DO A COMPLETE BALANCE OF THE
2542 /ELLIPSOMETER AND TYPE OUT THE RESULTS
2543
2544 2452 0000 BALE, Ø
2545 2453 1127 TAD POLCD /SET POL
2546 2454 4452 JMS I ASETM /CODE
2547 2455 4446 JMS I ABAL /BALANCE POL
2550 2456 1130 TAD ANZCD /SET ANZ

2551	2457	4452	JMS I ASETM	/CODE
2552	2460	4446	JMS I ABAL	/BALANCE ANZ
2553	2461	1127	TAD POLCD	/SET POL
2554	2462	4452	JMS I ASETM	/CODE
2555	2463	4446	JMS I ABAL	/BALANCE POL
2556	2464	4432	JMS I ASPACE	
2557	2465	4432	JMS I ASPACE	/TYPE 3 SPACES
2560	2466	4432	JMS I ASPACE	
2561	2467	4435	JMS I ARDSFT	/READ SHAFT ENCODER
2562	2470	1344	TAD CP	
2563	2471	4454	JMS I ABUFF	/TYPE "POL"
2564	2472	1345	TAD CO	
2565	2473	4454	JMS I ABUFF	
2566	2474	1346	TAD CLC	
2567	2475	4454	JMS I ABUFF	
2570	2476	4432	JMS I ASPACE	/LEAVE A SPACE
2571	2477	1100	TAD SHFTH	
2572	2500	4440	JMS I APRTDC	/PRINT OUT SHAFT
2573	2501	1101	TAD SHFTL	/ENCODER (POL)
2574	2502	4440	JMS I APRTDC	
2575	2503	4432	JMS I ASPACE	
2576	2504	4432	JMS I ASPACE	/LEAVE 3 SPACES
2577	2505	4432	JMS I ASPACE	
2600	2506	1347	TAD CA	
2601	2507	4454	JMS I ABUFF	/TYPE "ANZ"
2602	2510	1350	TAD CN	
2603	2511	4454	JMS I ABUFF	
2604	2512	1351	TAD CZ	
2605	2513	4454	JMS I ABUFF	
2606	2514	4432	JMS I ASPACE	/LEAVE A SPACE
2607	2515	1130	TAD ANZCD	/SET ANZ
2610	2516	4452	JMS I ASETM	/CODE
2611	2517	4446	JMS I ABAL	/BALANCE ANZ
2612	2520	1247	TAD CH1CD	/READ
2613	2521	4431	JMS I AANALG	/PHOTOMULTIPLIER
2614	2522	3352	DCA ESIG	/STORE
2615	2523	4435	JMS I ARDSFT	/READ SHAFT ENCODER
2616	2524	4451	JMS I AANZCP	/COMPLIMENT BY
2617	2525	1100	TAD SHFTH	/360.00
2620	2526	4440	JMS I APRTDC	/PRINT OUT SHAFT
2621	2527	1101	TAD SHFTL	/ENCODER (ANZ)
2622	2530	4440	JMS I APRTDC	
2623	2531	4432	JMS I ASPACE	
2624	2532	4432	JMS I ASPACE	
2625	2533	4432	JMS I ASPACE	/LEAVE 3 SPACES
2626	2534	1250	TAD CE	
2627	2535	4454	JMS I ABUFF	/TYPE "ES"
2630	2536	1251	TAD CS	
2631	2537	4454	JMS I ABUFF	
2632	2540	4432	JMS I ASPACE	/LEAVE SPACE
2633	2541	1352	TAD ESIG	/TYPE OUT ES
2634	2542	4437	JMS I APRTOC	
2635	2543	5652	JMP I BAIE	/EXIT - AC CLEAR
2636	2544	0320	CP,	320
2637	2545	0317	CO,	317
2640	2546	0314	CLC,	314
2641	2547	0301	CA,	301
2642	2550	0316	CN,	316
2643	2551	0332	CZ,	332
2644	2552	0000	ESIG,	0
2645			/	
2646			/	
2647				*2600

2650 /
2651 /
2652 /TO SET THE ANALYZER FROM THE KEYBOARD
2653 /
2654 2600 0000 SETAR, 0
2655 2601 4432 JMS I ASPACE
2656 2602 4432 JMS I ASPACE /TYPE TWO SPACES
2657 2603 4214 JMS RDFVE /READ A 5 DIGIT
2660 /BCD NUMBER
2661 2604 4460 JMS I ASETAN /USE SETAN ROUTINE
2662 2605 5600 JMP I SETAR /EXIT - AC CLEAR
2663 /
2664 /
2665 /TO SET THE POLARIZER FROM THE KEYBOARD
2666 /
2667 2606 0000 SETPR, 0
2670 2607 4432 JMS I ASPACE /TYPE TWO SPACES
2671 2610 4432 JMS I ASPACE
2672 2611 4214 JMS RDFVE /READ NUMBER
2673 2612 4461 JMS I ASETPL /USE SETPL
2674 2613 5606 JMP I SETPR /EXIT - AC CLEAR
2675 /
2676 /
2677 /TO READ A 5 DIGIT BCD CHARACTER FROM
2700 /THE KEYBOARD
2701 /
2702 2614 0000 RDFVE, 0
2703 2615 4455 JMS I AREADB /READ FIRST CHAR
2704 2616 7421 MQL
2705 2617 7701 ACL
2706 2620 4454 JMS I ABUFF /TYPE IT
2707 2621 7701 ACL
2710 2622 1300 TAD M260 /REMOVE ASKII CODE
2711 2623 7106 CLL RTL /ROTATE 4 BITS
2712 2624 7006 RTL /LEFT
2713 2625 3134 DCA DECH /STORE IN DECH
2714 2626 4455 JMS I AREADB /GET 2ND CHAR
2715 2627 7421 MQL
2716 2630 7701 ACL
2717 2631 4454 JMS I ABUFF /TYPE IT
2720 2632 7701 ACL
2721 2633 1300 TAD M260 /REMOVE ASKII
2722 2634 1134 TAD DECH
2723 2635 3134 DCA DECH /ADD TO DECH
2724 2636 4455 JMS I AREADB /GET 3RD CHAR
2725 2637 7421 MQL
2726 2640 7701 ACL
2727 2641 4454 JMS I ABUFF /TYPE IT
2730 2642 7701 ACL
2731 2643 1300 TAD M260 /REMOVE ASKII
2732 2644 7110 CLL RAR
2733 2645 7012 RTR /STORE IN HIGH
2734 2646 7012 RTR /ORDER 4 BITS OF
2735 2647 3133 DCA DECL /DECL
2736 2650 4455 JMS I AREADB /GET 4TH CHAR
2737 2651 7421 MQL
2740 2652 7701 ACL
2741 2653 4454 JMS I ABUFF /TYPE IT
2742 2654 7701 ACL
2743 2655 1300 TAD M260 /REMOVE ASKII
2744 2656 7106 CLL RTL /STORE IN MIDDLE
2745 2657 7006 RTL /4 BITS OF
2746 2660 1133 TAD DECL /DECL

2747	2661	3133	DCA DECL	
2750	2662	4455	JMS I AREADB	/GET LAST CHAR
2751	2663	7421	MQL	
2752	2664	7701	ACL	
2753	2665	4454	JMS I ABUFF	/TYPE IT
2754	2666	7701	ACL	
2755	2667	1300	TAD M260	/REMOVE ASKII
2756	2670	1133	TAD DECL	/STORE IN LOW
2757	2671	3133	DCA DECL	/4 BITS OF DECL
2760	2672	4457	JMS I ADPDBN	/CONVERT TO BIN
2761	2673	1126	TAD CH	
2762	2674	3136	DCA DESTH	/STORE IN
2763	2675	1125	TAD CL	/DESTINATION
2764	2676	3135	DCA DESTL	((DESTH, DESTL)
2765	2677	5614	JMP I RDFVE	/EXIT - AC CLEAR
2766	2700	7520	M260, -260	
2767			/	
2770			/	
2771			*3000	
2772			/	
2773			/	
2774			/TO MOVE MOTORS FROM KYBRD	
2775			/	
2776	3000	0009	MOTR,	0
2777	3001	4432	JMS I ASPACE	/TYPE SPACE
3000	3002	4455	JMS I AREADB	/GET FR CHAR
3001	3003	7421	MQL	/SAVE
3002	3004	7701	ACL	
3003	3005	4454	JMS I ABUFF	/TYPE FR CHAR
3004	3006	4432	JMS I ASPACE	/TYPE SPACE
3005	3007	1300	TAD MOTINF	/INTERROGATE XY
3006	3010	1301	TAD MX	
3007	3011	7640	SZA CLA	
3010	3012	5231	JMP YM	/XY IS NOT X
3011	3013	7701	ACL	/XY IS X
3012	3014	1302	TAD MF	/INTERROGATE
3013				/FOR REV CHAR
3014	3015	7640	SZA CLA	
3015	3016	5222	JMP MXR	/FR IS NOT F
3016	3017	1131	TAD M2XCD	/FR IS F - SET
3017	3020	4452	JMS I ASETM	/MOTORS X-FOR
3020	3021	5252	JMP RUNM	/RUN MOTORS
3021	3022	7701	MXR, ACL	/LOAD FR CHAR
3022	3023	1303	TAD MR	/IS IT R
3023	3024	7640	SZA CLA	
3024	3025	5600	JMP I MOTR	/NO - EXIT
3025	3026	1304	TAD M2XCDR	/YES - SET MOTORS
3026	3027	4452	JMS I ASETM	/TO X-REV
3027	3030	5252	JMP RUNM	/RUN MOTORS
3030	3031	1300	YM, TAD MOTINF	/IS XY CHAR Y
3031	3032	1305	TAD MY	
3032	3033	7640	SZA CLA	
3033	3034	5600	JMP I MOTR	/NO - EXIT
3034	3035	7701	ACL	/YES GET FR CHAR
3035	3036	1302	TAD MF	
3036	3037	7640	SZA CLA	
3037	3040	5244	JMP MYR	
3040	3041	1132	TAD M2YCD	/ SAME FOR Y
3041	3042	4452	JMS I ASETM	/ AS FOR X
3042	3043	5252	JMP RUNM	
3043	3044	7701	MYR, ACL	
3044	3045	1303	TAD MR	
3045	3046	7640	SZA CLA	

3046	3047	5680	JMP I MOTR	
3047	3050	1306	TAD M2YCDR	
3050	3051	4452	JMS I ASETM	
3051	3052	4455	RUNM,	JMS I AREADB /READ FIRST OF
3052	3053	1307	TAD M260M	/TWO DIGITS TO
3053	3054	7106	CLL RTL	/DETERMINE NO
3054	3055	7006	RTL	/OF 1/16" TO
3055	3056	3310	DCA SIXTN	/PLATES
3056	3057	4455	JMS I AREADB	
3057	3060	1307	TAD M260M	
3060	3061	1310	TAD SIXTN	
3061	3062	7421	MQL	
3062	3063	7701	ACL	/SAVE
3063	3064	4432	JMS I ASPACE	/TYPE SPACE
3064	3065	7701	ACL	
3065	3066	4440	JMS I APRTDC	/TYPE OUT MOVE-
3066				/MENT OF PLATES
3067	3067	7701	ACL	
3070	3070	4442	JMS I ADCBIN	/CONVERT MOVE-
3071				/ENT TO BINARY
3072	3071	7041	CIA	/SET UP COUNTER
3073	3072	3310	DCA SIXTN	
3074	3073	1311	TAD SIXTEN	
3075	3074	4444	JMS I AMOVE	/STEP 1/16"
3076	3075	2310	ISZ SIXTN	/STEP REQUIRED
3077	3076	5273	JMP -3	/NO OF 1/16"
3100	3077	5600	JMP I MOTR	/EXIT - AC CLEAR
3101	3100	0000	MOTINF, 0	
3102	3101	7450	MX, -330	
3103	3102	7472	MF, -306	
3104	3103	7456	MR, -322	
3105	3104	0300	M2XCDR, 300	
3106	3105	7447	MY, -331	
3107	3106	0060	M2YCDR, 60	
3110	3107	7520	M260M, -260	
3111	3110	0000	SIXTN, 0	
3112	3111	2000	SIXTEN, 2000	
3113	3112	0330	MXC, 330	
3114	3113	0331	MYC, 331	
3115			/	
3116			/	
3117			/TO MOVE X MOTOR	
3120			/	
3121	3114	0000	MOTRX, 0	
3122	3115	7200	CLA	
3123	3116	1312	TAD MXC	/PUT "X" IN MOTOR
3124	3117	3300	DCA MOTINF	/INFO
3125	3120	4200	JMS MOTR	/USE MOTR ROUTINE
3126	3121	5714	JMP I MOTRX	/RETURN
3127			/	
3130			/	
3131			/TO MOVE Y MOTOR	
3132			/	
3133	3122	0000	MOTRY, 0	
3134	3123	7200	CLA	
3135	3124	1313	TAD MYC	/PUT "Y" IN MOTOR
3136	3125	3300	DCA MOTINF	/INFO
3137	3126	4200	JMS MOTR	/USE MOTR ROUTINE
3140	3127	5722	JMP I MOTRY	/RETURN
3141			/	
3142			/	
3143			*3200	
3144			/	

3145 /
3146 /TO OPEN SHUTTER AND WAIT FOR A BALANCE
3147 /
3150 3200 0000 STOP, 0
3151 3201 4455 JMS I AREADD /DETERMINE NO OF
3152 3202 3237 DCA STPNO /BALANCES
3153 3203 3240 DCA DNFLAG /CLEAR FLAG
3154 3204 4462 JMS I AONSW /OPEN SHUTTER
3155 3205 4243 JMS RDP4 /READ PHOTOMULT
3156 3206 3241 DCA SM1 /STORE READINGS
3157 3207 4243 LPSTP, JMS RDP4 /READ AGAIN
3160 3210 3242 DCA SM2 /STORE READINGS
3161 3211 1242 TAD SM2
3162 3212 7041 CIA
3163 3213 1241 TAD SM1 /SM1-SM2
3164 3214 7700 SMA CLA /TEST RESULT
3165 3215 5223 JMP UPHILL /READS INCRESE
3166 3216 7001 IAC /READS DECREASE
3167 3217 3240 DCA DNFLAG /SET FLAG
3170 3220 1242 TAD SM2 /REPLACE SM1
3171 3221 3241 DCA SM1 /BY SM2
3172 3222 5207 JMP LPSTP /LOOP
3173 3223 1237 UPHILL, TAD STPNO /LAST BAL?
3174 3224 7640 SZA CLA
3175 3225 5231 JMP CNTST /NO BAL AGAIN
3176 3226 1240 TAD DNFLAG /APPROACHING MIN?
3177 3227 7650 SNA CLA
3200 3230 5235 JMP ENDSTP /FININHED
3201 3231 3240 CNTST, DCA DNFLAG /CLEAR FLAG
3202 3232 1242 TAD SM2 /REPLACE SM1 BY
3203 3233 3241 DCA SM1 /SM2
3204 3234 5207 JMP LPSTP /LOOP
3205 3235 4463 ENDSTP, JMS I AOFFSW /CLOSE SHUTTER
3206 3236 5600 JMP I STOP /EXIT - AC CLEAR
3207 3237 0000 STPNO, 0
3210 3240 0000 DNFLAG, 0
3211 3241 0000 SM1, 0
3212 3242 0000 SM2, 0
3213 /
3214 /
3215 /TO READ AND SUM PHOTOMULT 4 TIMES
3216 / (SUM LEFT IN AC)
3217 /
3220 3243 0000 RDP4, 0
3221 3244 1255 TAD M4C
3222 3245 3254 DCA CNT4 /SET COUNTER
3223 3246 3256 DCA SUMPTO /CLEAR
3224 3247 4445 JMS I ARDPTO /READ PHOTOM
3225 3250 1256 TAD SUMPTO /ADD TO SUM
3226 3251 2254 ISZ CNT4 /FOURTH TIME?
3227 3252 5247 JMP -3
3230 3253 5643 JMP I RDP4 /EXIT SUM IN AC
3231 3254 0000 CNT4, 0
3232 3255 7774 M4C, -4
3233 3256 0000 SUMPTO, 0
3234 /
3235 /
3236 *3400
3237 /
3240 /
3241 /TO ITERROGATE KEYBOARD AND DECODE
3242 /COMMANDS
3243 /

3244	3400	4456	JMS I AINIT	/INITILIZE
3245	3401	4430	JMS I ACRLF	/CRLF
3246	3402	4455	STSYS,	JMS I AREADB /READ A CHAR
3247	3403	7421	MQL	/SAVE IT
3250	3404	7701	ACL	/LOAD IT
3251	3405	4454	JMS I ABUFF	/TYPE IT
3252	3406	7701	ACL	/LOAD AGAIN
3253	3407	1246	TAD KC300	/SUB 300
3254	3410	7002	BSW	/BYTE SWAP
3255	3411	3247	DCA CHARAD	/SAVE 1ST CHAR
3256	3412	4455	JMS I AREADB	/READ 2ND CHAR
3257	3413	7421	MQL	
3260	3414	7701	ACL	
3261	3415	4454	JMS I ABUFF	/TYPE IT
3262	3416	7701	ACL	
3263	3417	1246	TAD KC300	/SUBT 300
3264	3420	1247	TAD CHARAD	/PUT IN LOW BYTE
3265	3421	3247	DCA CHARAD	/WITH 1ST CHAR
3266	3422	1243	TAD STLST	/SET ADDRESS OF
3267	3423	3015	DCA LSTPT	/POINTER
3270	3424	1415	TAD I LSTPT	/GET COMPARISON
3271	3425	7041	CIA	/WORD. NEGATE
3272	3426	7450	SNA	/0 INDICATES END
3273	3427	5241	JMP ENDLST	/OF LIST
3274	3430	1247	TAD CHARAD	/COMPARE
3275	3431	7640	SZA CLA	/IF NOT THE SAME
3276	3432	5224	JMP .-6	/GET NEXT COMP
3277	3433	1015	TAD LSTPT	/ADDRESS OF LOC
3300	3434	1244	TAD ADLST	/IS SUMM
3301	3435	3245	DCA ADSTOR	/SAVE ADDRESS
3302	3436	1645	TAD I ADSTOR	/GET ADDRESS OF
3303	3437	3245	DCA ADSTOR	/COMMAND, SAVE IT
3304	3440	4645	JMS I ADSTOR	/EXECUTE COMMAND
3305	3441	4430	ENDLST,	JMS I ACRLF /CRLF ENDS COMMAND
3306	3442	5202	JMP STSYS	/START OVER
3307	3443	3677	STLST,	3677
3310	3444	0040	ADLST,	40
3311	3445	0000	ADSTOR,	0
3312	3446	7500	KC300,	-300
3313	3447	0000	CHARAD,	0
3314			/	
3315			/	
3316			*3700	
3317	3700	0205	ABE,	0205
3320	3701	0201	ABA,	0201
3321	3702	0220	ABP,	0220
3322	3703	2301	ASA,	2301
3323	3704	2320	ASP,	2320
3324	3705	1530	AMX,	1530
3325	3706	1531	AMY,	1531
3326	3707	2302	ASB,	2302
3327	3710	1723	AOS,	1723
3330	3711	0323	ACS,	0323
3331	3712	0000	AEND,	0
3332			/	
3333			/	
3334			*3740	
3335	3740	2452	BBE,	BALE
3336	3741	2406	BBA,	BALA
3337	3742	2400	BBP,	BALP
3340	3743	2600	BSA,	SETAR
3341	3744	2606	BSP,	SETPR
3342	3745	3114	BMX,	MOTRX

3343	3746	3122	BMY,	MOTRY
3344	3747	0064	BSB,	ASTOP
3345	3750	2276	BOS,	ONSW
3346	3751	2306	BCS,	OFFSW
3347			/	
3350			/	

NO ERRORS

AANALG	0031
AANZCP	0051
ABA	3701
ABAL	0046
ABE	3700
ABNBED	0041
ABP	3702
ABUFF	0054
ACCNTO	0702
ACCST	0667
ACCSTP	0716
ACCUM	0370
ACL	7701
ACOMP0	1727
ACOMP1	1730
ACOMP2	1731
ACRLF	0030
ACS	3711
ACTIME	0722
ADCBIN	0042
ADLST	3444
ADPADD	0050
ADPDBN	0057
ADPSUB	0047
ADSTOR	3445
AEND	3712
AH	0122
AHEAD	2060
AINIT	0056
AINTSR	0002
AKFLAG	0571
AKYCNT	0572
AL	0121
AMOVE	0044
AMULT5	0053
AMX	3705
AMY	3706
ANALG	0506
ANZCD	0130
ANZCP	0723
ANZ2	2167
AOFFSW	0063
AONSW	0062
AOS	3710
APOS0	1506
APOS1	1507
APOS2	1510
APOS3	1511
APOS4	1512
APRTDC	0040
APRTOC	0037
ARDDVM	0036
ARDPTO	0045
ARDSFT	0035

AREADB 0055
AREV 0043
ASA 3703
ASB 3707
ASETAN 0060
ASETM 0052
ASETPL 0061
ASP 3704
ASPACE 0032
ASTACK 1725
ASTEP 0033
ASTOP 0064
ASTORE 1726
ASUM 1724
ASUMH 0107
ASUML 0106
ATFLAG 0570
ATLCNT 0573
AWAIT 0034
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BAL 1600
BALA 2406
BALE 2452
BALLP1 1611
BALP 2400
BALU 2414
BSA 3741
BBE 3740
BBP 3742
BCS 3751
BH 0124
BHLDK 2177
BKWD 2166
BK2 1102
BK3 1124
BL 0123
BLFLAG 1723
BMX 3745
BMY 3746
BNBCD 1050
BNBR 1142
BNLP1 1055
BNLP2 1076
BNLP3 1120
BOS 3750
BSA 3743
BSB 3747
BSP 3744
BSW 7002
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BUFLP1 0253
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CHARAD 3447
CHDIR 1420
CH1CD 2447
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CLASWP 7721
CLC 2546
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CNT3HD	2244
CNT4	3254
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COMP1	1452
COMP2	1460
CP	2544
CRLF	0400
CS	2451
CTHUP	0244
CZ	2551
DCBIN	1000
DECH	0134
DECL	0133
DESTH	0136
DESTL	0135
DIG	1143
DIGCTR	0502
DIR	0110
DMSEH	2172
DMSEL	2171
DNFLAG	3240
DNUMB	0105
DPADD	1541
DPDBN	2200
DPSUB	1553
DPX2	2245
DPX2H	2240
DPX2L	2237
DPX5	2255
DPX5H	2242
DPX5L	2241
DVMH	0103
DVML	0102
ENDBUF	0362
ENDKBF	0365
ENDLST	3441
ENDSK1	1325
ENDSTK	0010
ENDSTP	3235
ENDTIM	0625
ESIG	2552
EXTINT	0213
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FNH3	1126
FWD	2165
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KBDCNT	0374
KCF	6030
KC10	1146
KC100	1145

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KC3 0593
KC300 3446
KC4 0477
KK1777 0566
KK2177 0567
KPDPS 1571
KYBDPT 0013
KYBRD 0302
KYFLAG 0367
KYND2 0347
KYNEND 0314
K1000D 0745
K212 0414
K215 0415
K240 0416
K260 0476
K35D 0746
LINK 0371
LKPRT 0574
LPSTP 3207
LPSUM 1335
LSTPT 0015
L180 2174
L360 2176
MASK 0473
MASK17 0504
MASK37 0653
MASK49 0652
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MK7400 1027
MK77 0541
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MLT100 1044
MNBR 1043
MOTINF 3100
MOTOR 1434
MOTR 3000
MOTRX 3114
MOTRY 3122
MOVE 1435
MQA 7501
MQL 7421
MQSAVE 0372
MR 3103
MSDIG 0104
MSKDIR 1416
MSKDRI 1432
MSKDR2 1417
MSKD1 0715
MULT10 1030
MULT5 1034
MVEFWD 2126
MX 3101
MXC 3112
MXR 3022
MY 3105
MYC 3113

MYR 3044
M2XCD 0131
M2XCDR 3104
M2YCD 0132
M2YCDR 3106
M260 2700
M260M 3107
M4C 3255
NOTEDB 0271
NOTEND 0241
NUMBER 0500
OCNBR 1024
OFFSW 2306
ONSW 2276
PHTOCD 1354
POLCD 0127
POL2 2170
POSCT 1721
POS0 1622
POS1 1625
POS2 1633
POS3 1660
POS4 1713
PRINT 0417
PRTDC 0447
PRTOC 0461
RDDVM 0635
RDFVE 2614
RDPTO 1347
RDP4 3243
RDSFT 0626
READB 0330
READPT 0014
REV 1400
ROTNBR 0474
RUNM 3052
SETAN 2143
SETAR 2600
SETEL 2000
SETKFL 0324
SETM 1421
SETPL 2154
SETPR 2606
SHFTH 0100
SHFTL 0101
SHIGH 0542
SIXTEN 3111
SIXTN 3110
SKC16 0717
SM1 3241
SM2 3242
SPACE 0407
SPF 6040
STACK 1300
STBL 1603
STBUF 0363
STEP 0654
STEP1 0600
STKL 0111
STKLC 0112
STKYBF 0366
STLP1 1523
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STOP	3200
STORE	1513
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STPNO	3237
STRROT	0505
STSTK	0120
STSYS	3402
SUBPT	2027
SUM	1326
SUMH1	0113
SUMH2	0114
SUML1	0115
SUML2	0116
SUMPTO	3256
SUSTK1	1323
SUSTK2	1324
SWP	7521
S2GTS1	1504
S2LTS1	1505
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TELTP	0223
TFLAG	0364
TYPEPT	0012
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WTIME	0721
WTI	0720
YM	3031