Small-sample Probabilistic Simulation Software Tool FReET

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ABSTRACT: The objective of the paper is to present methods and software for the efficient statistical, sensitivity and reliability assessment of infrastructure. A special attention is devoted to small-sample simulation techniques which have been developed for the analysis of computationally intensive problems. The paper shows the possibility of "randomizing" computationally intensive problems in the sense of the Monte Carlo type simulation. In order to keep the number of required simulations at an acceptable level, optimized Latin Hypercube Sampling is utilized. The technique is used for simulation of random variables and random fields. Sensitivity analysis is based on nonparametric rank-order correlation coefficients. Statistical correlation is imposed by the stochastic optimization technique – simulated annealing. A hierarchical sampling approach has been developed for the extension of the sample size in Latin Hypercube Sampling, enabling the addition of simulations to a current sample set while maintaining the desired correlation structure. The paper continues with a brief description of the user-friendly implementation of the theory within FReET commercial multipurpose reliability software.

1. INTRODUCTION
The presence of uncertainty in the analysis and design of engineering systems has always been recognized. Uncertainties are involved in every part of the system – Structure – Load – Environment. Traditional approaches simplified the problem by considering the uncertain parameters to be deterministic, and accounted for the uncertainties through the use of partial safety factors in the context of limit states. Such approaches do not guarantee the required reliability and they do not provide information on the reliability achieved and/or on the influence of individual parameters on reliability. Therefore, in recent years, attention is being given to fully probabilistic approaches and software tools which can be used for such purposes. Important topics can thus be treated in an advanced manner, e.g. the probabilistic vulnerability assessment of civil infrastructure systems followed by efficient decision-making processes.

The standard definition of an engineering problem featuring uncertainty or randomness, which is to be analyzed using computers, is as follows. A random response of the studied engineering system (e.g. a structure) is represented by random variable \( Z \). In statistical analyses, \( Z \) may represent a random response of a system (e.g. deflection, stress, ultimate capacity, etc.) or, in reliability calculations; \( Z \) is called a safety margin. Random variable \( Z \) is a function of basic random variables \( X = X_1, X_2, \ldots, X_n \) (or random fields):

\[
Z = g(X)
\]  

where the function \( g(X) \), a computational model, is a function of a random vector \( X \) (and also of other, deterministic quantities). Random vector \( X \) follows a joint probability distribution function (PDF) \( f_X(X) \) and, in general, its marginal variables can be statistically correlated. This pa-
per deals with situations when the information about $f_X(X)$ is limited to the knowledge of univariate marginal distributions $f_1(x), \ldots, f_{N_{var}}(x)$ and a correlation matrix, $T$ (a symmetric square matrix of order $N_{var}$). The output variable (or generally a vector) $Z$ represents a transformed variable and the task is to perform statistical, sensitivity and possibly reliability analyses upon it. It is assumed that the analytical analysis of the transformation of input variables to $Z$ is not possible.

Approaches focused on the estimation of statistical moments of response quantities, such as means or variances, are commonly termed statistical analyses. In sensitivity analysis, approaches aiming at the quantification of the sensitivity of output (response, failure probability) to variations in input variables are applied. The main result of reliability analysis is an estimate of the theoretical failure probability.

If $g(X)$ represents a failure condition, then it is called the limit state function and $Z$ becomes the safety margin. Usually, the convention is that it takes a negative value if a failure event occurs; $Z \leq 0$, and a survival event is defined as $Z = g(X) > 0$. The limit state function can be an explicit or implicit function of basic random variables and it can take either a simple or a rather complicated form (e.g. a computer program). The performance of the system and its components may be described considering a number of limit states (multiple limit state functions). The aim of reliability analysis is the estimate of unreliability using a probability measure called the theoretical failure probability, defined as

$$p_f = P(Z \leq 0). \quad (2)$$

This failure probability is again calculated as a probabilistic integral:

$$p_f = \int I[g(X)] f_X(X) dX = \int_{D_f} f_X(X) dX \quad (3)$$

The function $I[g(X)]$ is an indicator function that equals one for failure event ($g \leq 0$) and zero otherwise. In this way, the domain of integration of the joint PDF above is limited to the failure domain $D_f$ where $g(X) \leq 0$.

The explicit calculation of the failure probability integral in Eq. (3) is generally impossible. A large number of efficient stochastic analysis methods have therefore been developed during the last seven decades.

A straightforward solution for these tasks is numerical simulation. The interest in simulation methods started in the early 1940’s with the purpose of developing inexpensive techniques for testing engineering systems by imitating their real behavior. These methods are commonly called Monte Carlo simulation techniques. The principle behind the method is to develop an analytical model – a computer based response or limit state function (Eq. 1) that predicts the behavior of the studied system and repeats it many times under all possible conditions. This simulation principle has remained formally the same up until the present day.

The common feature of the many different techniques covering all the above-mentioned categories is the fact that they require repetitive evaluation (simulation) of the response or limit state function $g(X)$. The development of methods is from a historical perspective a struggle to decrease the amount of simulations, or avoid an excessive number of them. Crude Monte Carlo simulation cannot be applied to time-consuming problems, as it requires a large number of simulations (the repeated calculation of structural response) to deliver statistically significant estimates of the outputs.

In the context of reliability analyses, this obstacle was historically successfully solved for by the approximation techniques FORM and SORM, e.g. (Hasofer and Lind 1974, Madsen et al. 1986). In spite of some problems concerning accuracy, these techniques are widely accepted today and have become in some cases standard tools in code calibration. Once this was achieved, research then focused on the development of
advanced simulation techniques which concentrate simulations in the failure region (Schuëller 1998). Among the many efficient methods developed during the last decades, Latin Hypercube Sampling and response surface methodologies are often used for computationally demanding continuum mechanics problems.

The objective of the paper is to present methods for efficient statistical, sensitivity and reliability assessment implemented in FReET software (Novák et al. 2013, 2014). Attention is given to those techniques that have been developed for the analysis of computationally intensive problems; nonlinear FEM analysis being a typical example. The paper shows the possibility of “randomizing” computational tasks in the sense of the Monte Carlo type of simulation. The stratified simulation technique Latin Hypercube Sampling is used in order to achieve variance reduction of the estimated outputs at a given number of simulations.

The paper contains basic information on FReET software and the implemented methods with relevant references.

2. UNCERTAINTY SIMULATION

2.1. A small-sample Monte Carlo type simulation

For time-intensive calculations, small-sample simulation techniques based on stratified sampling of the Monte Carlo type represent a rational compromise between feasibility and accuracy. Therefore, Latin Hypercube Sampling (LHS) (Conover 1975, McKay et al. 1979, Novák et al. 1998), which is well known today, has been selected as a key fundamental technique. LHS belongs to the category of advanced stratified sampling techniques which result in the very good estimate of statistical moments of response using small-sample simulation. More accurately, LHS is considered to be a variance reduction technique, as it yields lower variance in statistical moment estimates compared to crude Monte Carlo at the same sample size. This is the reason the technique became very attractive for dealing with computationally intensive problems like e.g. complex finite element simulations.

2.2. Statistical correlation control

Once \( N_{\text{sim}} \) samples of each marginal variable are generated, separately, the correlation structure prescribed by the target correlation matrix must be taken into account. There are generally two problems related to the statistical correlation: First, during sampling an undesired correlation can occur between the random variables (Vořechovský, 2012). For example, instead of a correlation coefficient of zero for the uncorrelated random variables an undesired correlation of eg. 0.4 can be generated. This can happen especially in the case that only a very small number of simulations (in the order of tens) are carried out (in the order of tens), where the number of interval combinations is rather limited. The second task is to introduce the prescribed statistical correlation between the random variables defined by the correlation matrix. This can be achieved by rearranging the order of samples of each variable in the LHS simulation plan in such a way that either they diminish the undesired random correlation when unit matrix \( T \) is required or they introduce a target correlation structure. Such a rearrangement of the sample ordering can be achieved via several different techniques published in the literature on LHS (e.g. Iman and Conover 1982, Owen 1994); however, some serious limitations have been found by the authors while using them.

A robust technique to impose statistical correlation based on the stochastic method of optimization called simulated annealing has been proposed by Vořechovský and Novák (2009). Extensive studies on the performance of the algorithm (Vořechovský 2011) show that it performs considerably better than other widely used algorithms for correlation control, namely both Iman and Conover’s (1982) Cholesky decomposition and Owen’s (1994) Gram-Schmidt orthogonalization.

2.3. Hierarchical sampling

When using Monte Carlo-type simulation, the adequacy of a given sample for the purpose of giving acceptable estimates of desired statistical quantities cannot be determined a priori, and thus
the ability to extend or refine an experimental design may be important. This can be done very easily in crude Monte Carlo sampling. Very often, though, running each realization (as either a physical or virtual experiment) is very expensive. In conventional Latin Hypercube Sampling, however, it is necessary to specify the number of simulations in advance. If too small a sample set is used (i.e., a set that does not give acceptable statistical results), the analyst normally has to abandon the results and run new analyses with a larger sample set. It is thus desirable to start with a small sample and then extend (or refine) the design if deemed necessary. The extension would permit the use of a larger sample set without the loss of any of the already performed, and possibly quite expensive, calculations.

This problem has been overcome by the method called Hierarchical Latin Hypercube Sampling, which was proposed recently in (Vořechovský 2009, 2014). Note that a similar solution has been published in (Sallaberry et al. 2008). The method combines the addition of simulations to the current sample set (hierarchical refinement of sampling probabilities) while maintaining the desired correlation structure by employing an advanced correlation control algorithm (Vořechovský and Novák, 2009) for the extended part of the sample. The initial LH-sample can have an arbitrary number of simulations and the added sample must have an even integer times more sampling points than the current sample size (e.g., twice more). Numerical studies presented in (Vořechovský 2014) have shown that the extended sample has all the properties that the same LH sample would have when simulated in a single LHS run. The advantage in sample size flexibility is obvious.

2.4. Sensitivity and reliability analyses
An important task in structural reliability analysis is to determine the significance of random variables. With respect to the small-sample simulation techniques described above the most straightforward and simplest approach uses the non-parametric rank-order statistical correlation between the basic random variables and the structural response variable (Iman and Conover 1980, Novák et al. 1993). The sensitivity analysis is obtained as an additional result of LHS, and no additional computational effort is necessary.

The relative effect of each basic variable on the structural response can be measured using the partial correlation coefficient between each basic input variable and the response variable. The method is based on the assumption that the random variable which influences the response variable most considerably (either in a positive or negative sense) will have a higher correlation coefficient than the other variables. Because the model for the structural response is generally nonlinear, a non-parametric rank-order correlation is used by means of the Spearman correlation coefficient or Kendall tau. Sensitivity analysis can be depicted using parallel coordinates (Inselberg, 2009); a strong positive influence (high correlation coefficient) results in parallel lines between the input variable and the response variable, while a strong negative influence results in a bundle of intersecting lines.

In cases when we are constrained by the use of only a small number of simulations (tens, hundreds) it can be difficult to estimate the failure probability. The following approaches are therefore utilized here; they are approximately ordered from elementary (extremely small number of simulations, inaccurate) to more advanced techniques:

- Cornell’s reliability index – calculation of the reliability index from an estimate of the statistical characteristics of the safety margin,
- The curve fitting approach – based on the selection of the most suitable probability distribution of the safety margin,
- FORM approximation (Hasofer-Lind’s index),
- Importance sampling techniques,
- Response surface methods.

These approaches are not described here as they are well-known in the reliability literature, and also the provision of all details is beyond the aim of this paper. In some cases, these tech-
niques do not always belong to the category of very accurate reliability techniques (especially the first three in the list). However, they represent a feasible alternative in many practical cases.

3. FREET SOFTWARE

FReET, the multipurpose probabilistic software for the statistical, sensitivity and reliability analysis of engineering problems (Novák, Vořechovský and Rusina – Novák et al. 2003, 2009, 2013) is based on the efficient reliability techniques described above. There are three basic parts:

The “Random Variables” window (Figure 1) allows the user-friendly input of basic random variables of the analyzed problem. Uncertainties are modeled as random variables described by their probability density functions (PDF). The user can choose from a set of selected theoretical models such as normal, lognormal, Weibull, rectangular, etc. Random variables can be described in three ways. The first option is to describe them by their statistical characteristics (statistical moments): the mean value, standard deviation (or coefficient of variation), coefficient of skewness and kurtosis excess. Alternatively, they can be set based on their parameters or on a combination of parameters and moments. The number of free parameters is identical in all three modes (moments, parameters or a mixture of both) and it represents the “degrees of freedom” of the distribution. A special feature is enabled: the user can work with a variable that represents the $i$-th greatest or smallest variable of $n$ independent and identically distributed (iid) variables selected from the basic (elemental) distribution (order statistics). In this way, e.g. the smallest of the $n$ iid random variables can be selected and the software works with this transformed distribution as if this was on the list of available elemental distributions. This feature is accessible from the “Distribution details” window and this window also provides the option of performing basic computations with a single random variable.

Another option allowing definition of the distribution of a single random variable is to use raw data. Upon loading an arbitrary list of values, the program either enables the use of a histogram or proposes the best matching available parametric distribution based on the Kolmogorov-Smirnov test.

The “Statistical Correlation” window serves for the input of target correlation matrix $T$. The user can work at the level of a subset of correlation matrices (each related to a group of random variables) or at the global level (all random variables resulting in a large correlation matrix). The level of correlation during interactive input is highlighted, and the positive definiteness is checked. Note that Simulated Annealing applied for correlation control does not require the positive definiteness as it automatically delivers a sample having the nearest positive semidefinite correlation matrix to the target matrix $T$.

Random input parameters are generated according to their PDF using LHS sampling. Samples are reordered by the Simulated Annealing approach in order to match the required correlation matrix as closely as possible. Generated realizations of random parameters are used as inputs for the analyzed function (computational model). The solution is performed $N_{\text{sim}}$ times and the results (structural response) are saved. At the end of the whole simulation process the resulting set of structural responses is statistically evaluated. The results are: estimates of the mean value, variance, coefficient of skewness and kurtosis, and the empirical cumulative probability density function estimated by an empirical histogram of structural response. This basic statistical assessment is visualized through the “Histograms” window. It is followed by reliability analysis based on several approximation techniques: (i) the basic estimate of reliability by the Cornell safety index, (ii) the curve fitting approach applied to the computed empirical histogram of response variables and (iii) the simple estimate of probability of failure based on the ratio of failed trials to the total number of simulations.

Additional information regarding the problem solved is obtained via the sensitivity analysis of each response function based on its rank-order
correlation coefficient. Even though this is actually a byproduct of the simulation which does not require any special additional effort, it provides very useful information in many cases. If the correlation coefficient between a certain input variable and output variables is close to zero, we can conclude that the input variable has (in its simulated range) a small or even negligible effect on the output. This can sometimes help to decrease the probabilistic dimension of the problem because such an input can be considered deterministic.

3.1. Summary of main features
State-of-the-art probabilistic algorithms are implemented in FReET to compute the probabilistic response and reliability. FReET is a modular computer system for performing probabilistic analysis developed mainly for computationally intensive deterministic modeling and the running of user-defined subroutines. The main features of the software are:

3.1.1. Stochastic model (inputs)
The fundamental part of the software is the user-friendly handling of inputs – basic random variables and theirs statistical correlation. The main features are:

- A friendly Graphical User Environment (GUE).
- 30 probability distribution functions (PDF), mostly 2-parametric, some 3-parametric, two 4-parametric (Beta PDF and normal PDF with a Weibullian left tail).
- Unified description of random variables with the optional use of statistical moments or parameters or a combination of moments and parameters.
- PDF calculator.
- Extreme value distributions and order statistics for any available parametric distribution.
- Statistical correlation (there is also a weighting option).
- Categories and comparative values for PDFs.
- Visualization of basic random variables, including statistical correlation in both Cartesian and parallel coordinates.

3.1.2. Response/Limit state function
The user has several options to define the analyzed function. The complexity of the task is decisive for the selection of an appropriate interface. Several efficient and user-friendly options are implemented:

- Closed form (direct), using the implemented Equation Editor (simple problems).
- Numerical (indirect), using a user-defined DLL function that can be prepared in practically any programming language (C++, Fortran, Delphi, etc.).
- General interface to third-party software using user-defined *.BAT or *.EXE programs based on input and output text communication files.
- Multiple response functions assessed in the same simulation run.

3.1.3. Results (outputs)
The assessment of outputs (the results of Monte Carlo-type simulation) consists of:

- Histograms of output variables.
- Sensitivity analyses.
- Reliability estimates by various simulation and approximation methods.
- Limit state functions.
- Parametric studies.
- Cost/Risk assessment.

3.1.4. Probabilistic techniques
Both standard and advanced statistical, simulation and reliability techniques are implemented:

- Crude Monte Carlo simulation.
- Latin Hypercube Sampling (3 alternatives).
- Hierarchical Latin Hypercube Sampling (extension of sample size).
- First Order Reliability Method (FORM).
- Curve fitting.
- Simulated Annealing employed for correlation control over inputs.
• Bayesian updating.
• Response surface.
• Importance sampling around mean values.

Figure 1: “Random variables” window (above); “Reliability” window with empirical histogram, Curve fitting, Cornell safety index and Monte Carlo sampling estimates (below).

4. CONCLUSION
The paper describes the main software features and stochastic methods implemented in FReET software. Efficient techniques of employing stochastic simulation methods were combined in order to offer an advanced tool for the probabilistic assessment of user-defined problems at ultimate capacity and serviceability limit states.

The presented software tools may be applied in the advanced design of structures, when making decisions about alternatives, when searching for optimum life-cycle cost solutions, and in cost-effective decision-making processes concerning maintenance inspection and planning. With regard to this, the time aspect emphasizes the urgent need for durability limit state consideration.

Real world engineering structural design, development and assessment is very challenging as it is subjected to a whole host of sources of variation. Probabilistic techniques are therefore used in various engineering fields, offering advantages over the alternative, but more traditional, deterministic methods that might otherwise be employed. Small-sample probabilistic simulation of the Monte Carlo type can address a lot of the shortcomings of classical deterministic approaches and a ready-to-use software program has been developed for the analysis of any user-defined problem. Its wide range of applicability, both practical and theoretical, provides the opportunity for further intensive development of the software tools.

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6. REFERENCES


